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DELINEATION OF A WAVE CLIMATE

FOR

DAM NECK, VIRGINIA BEACH, VIRGINIA

by

Andrew L. Gutman

Special Report in Applied Marine Science and Ocean Engineering (SRAMSOE) No. 125

Virginia Institute of Marine Science Gloucester Point, Virginia 23062 William J. Hargis, Jr., Director

December 1976



SUMMARY

A total of 78,449 wave observations from six sources, which vary widely in format duration, biases, and quality are compiled in this report (Figs. 1 and 2):

a) Shipboard wave observations for a 1° Marsden Square 116-subsquare 65 (14,580 observations during 12/48-12/73).

b) Chesapeake Lightship wave observations (3977 observations during 1/70-12/72).

c) Coastal Engineering Research Center-Coast Guard Cooperative Surf Observation Program (25,338 observations during 4/54-12/65).

d) Virginia Beach wave gage (6,354 observations during 4/64-10/69).

e) Virginia Institute of Marine Science-Coastal Engineering Research Center Voluntary Wave Observer Program (1882 observations during 6/74-8/76).

f) Hindcasted wave (SMB by Saville, 1954) for Chesapeake Light (26,260 wave computations during 1/48-12/50).

The principal descriptor of wave height used here is the "significant wave height", which is defined as the average height of the highest 33% of the waves occurring during a particular sampling period.

Conclusions resulting from the thorough synthesis and comparison of these wave data are:

 After evaluation of the limitations and biases of all the above listed data sources, the Virginia Beach wave gage data is determined to be the most reliable, useful and representative source for delineating the nearshore wave climatology for the proposed Dam Neck Ocean Outfall.
Only a slight seasonality of wave height and direction is indicated by the six data sources:

a) The mean wave heights during the summer (April-August) are lower than waves during the winter. (September-March) by about 0.1 to 1.5 feet depending on the source.

b) The dominant direction of wave approach is from the Southeast and East during the summer and from the Northeast and East during the winter.

3) Wave periods are unreliable for all sources but the gage, because all the observed wave period data show large apparent biases towards lower wave periods and lack any apparent trends.

4) The mean wave heights of the six data sources show a landward decrease, which would be expected for waves traveling across the shelf, lending credence to the data and this synthesis.

5) The extreme wave climate constructed from the Virginia Beach gage data (located at a depth of 20 feet) is:

a) 68% of all significant wave heights (H_s) were less than 4.2 feet and 99.7% were less than 9.5 feet.

b) The highest significant height measured at the gage during the period of record was $H_s = 11.5$ feet.

c) The highest significant wave height likely to occur in the Virginia Beach, Dam Neck area, in 27 years, extrapolated from a frequency of occurrence curve, was determined to be $H_s = 13.5$ feet.

6) From previous wave refraction data, comparisons of nearshore and offshore wave data sources, previous storm occurrences, and gage characteristics, it is determined that the data recorded at the Virginia Beach wave gage is representative of wave events which are likely to occur adjacent to Dam Neck in 30 feet of water. Thus, monthly summaries of these data are presented in the Appendix, as a further aid to the engineer.

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DELINEATION OF A WAVE CLIMATE

FOR

DAM NECK, VIRGINIA BEACH, VIRGINIA

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Andrew L. Gutman

December 1976

PREFACE

This report has been prepared at VIMS under contract with Malcolm Pirnie Engineers, Inc., Newport News, Virginia, by Andrew L. Gutman under the supervision of Dr. Victor Goldsmith and Dr. Robert J. Byrne, in response to a request for detailed wave information to be used by others in planning a proposed sewage ocean outfall pipeline and diffuser to be located off Dam Neck, Virginia. These wave data will be useful for the design of the outfall structure, as well as optimal utilization of construction vessels during the emplacement of the outfall pipe.

The data and results presented in this report are derived from information supplied by several sources:

1) N.O.A.A. Environmental Data Service provided shipboard and Chesapeake Lightship wave data.

2) The U.S. Army Corps of Engineers Coastal Engineering Research Center provided the wave data from the Virginia Beach Gage, the Cooperative Surf Observation Program, and the VIMS-CERC Voluntary Surf Observer Program.

3) The SMB Hindcast wave data comes from the Beach Erosion Board (now C.E.R.C.) T.M. #55 by Thorndike Saville Jr., (1954).

4) Storm data was provided by W.S. Richardson of the Techniques Development Lab., U.S. Weather Service (N.O.A.A.) and the Norfolk Station National Weather Service office.

A.E. DeWall and E. Thompson of CERC were particularly helpful in supplying wave data.

Robert Gregory assisted in the computations.

DATA SOURCES AND METHODS

DESCRIPTION OF WAVES

If an observer is given the task of visually describing the wave height and/or wave period on the ocean surface or at the shoreline, the difficulties of estimation soon become apparent. The reason the exact specification of the wave height and period is difficult is that the sea surface, at any given time or place, is composed of many different wave "trains" with different heights and periods. Furthermore, each of these component waves is moving at a different speed so that the faster components move through the slower ones. The result is that the sea surface is always confused. The problem the observer faces is to characterize the confusion in some meaningful and internally consistent fashion.

Research on ocean waves indicates that the distribution of wave heights passing a point do conform, more or less, with known statistical distributions. As a result it has been possible to estimate various characteristics of these distributions. A schematic representation of a frequency distribution of wave heights passing an observation point over some short time interval is shown in Figure 1d. Also shown is some of the parameters useful in engineering work. In particular we will make use of $H_{1/3}$ and $H_{1/10}$. $H_{1/3}$ (= H_s) is called the "significant wave height" and it is defined as the average of the waves in the upper 33% of the distribution.

In addition to these parameters the significant wave period, T_s , is considered. This is generally a semi-subjective average period of the most prominent waves.

Of the data sources previously listed only the recording wave gage data can be formally treated to obtain H_s and T_s . The other data sources gives visually estimated values of H_s . Experience has shown that an observer at sea, when estimating wave heights, estimates a value close to H_s . These parameters are discussed further in later sections.

COOPERATIVE SURF OBSERVATION PROGRAM

25,338 wave observations were accumulated between 4/54-12/65 at Virginia Beach in this Coast Guard-Coastal Engineering Research Center Project. In this program T_s was estimated by counting the time of passage of eleven wave crests (10 complete breakers) and then dividing by ten. Significant wave height (H_s) was estimated by recording the average height of the highest third of the breakers. Wave direction was recorded as the direction from which the most prominent waves were coming just before they broke. Observations were taken every four hours, recorded on coded forms and then sent to CERC. A sample form complete with instructions for the wave observer is included in the appendix to this report.

Table 1 outlines the many problems associated with such an observation program. It is concluded that this data should be only applied in the Virginia Beach area and the data should

not be used to determine structural design. However, the data is useful in that it represents an unusually long period of record and can be used in conjunction with other, more seaward, data.

VIRGINIA INSTITUTE OF MARINE SCIENCE-COASTAL ENGINEERING RESEARCH CENTER VOLUNTARY WAVE OBSERVER PROGRAM

Some 1,882 wave observations along the coast from Virginia Beach, Virginia to Currituck Light, North Carolina were gathered. between January, 1975 and August, 1976 at ten locations (Fig. 1). Estimates of significant wave height and period were determined as described for the COSOP Program (above). However, observations were not taken every four hours but on a daily basis, usually five days/week Monday through Friday. In addition, data was derived along the coast at 10 separate locations at highly sporadic intervals, as opposed to one location for the COSOP Program (Figure 2).

As indicated in Table 1, these data are of little use in delineating a wave climate of use for engineering design and planning. It does, however, provide some estimate of the long shore variation of wave energy along the coast.

A sample form complete with instructions for the wave observer is included in the appendix to this report.

SHIP WAVE OBSERVATIONS

Wave information stored on magnetic tape by N.O.A.A. Environmental Data Service for Marsden one degree subsquare

SS-65 within Marsden 1° degree square 116 (Fig. 1) adjacent to the study area consisted of 14,580 observations accumulated during 12/48-12/73.

Shipboard wave observers (NOAA, 1964) are instructed to select a patch of foam or similar floating material, and divide the elapsed time of passage of ten or fifteen wave crests through the foam by the number of crests, to estimate a wave period. Wave height is determined by comparison to a known object on the ship. It is assumed that these estimates represent significant wave height and period. Shipboard wave observers are generally untrained and often rely on experience rather than actual time or height measurements to estimate the wave parameters.

Thompson and Harris (1972) have discussed errors involved with shipboard wave observations (see Table 1). As with all observer programs, much error and bias must be assumed when interpreting the data. Nevertheless, shipboard wave observations fill a gap by providing a deepwater wave climatology. As will be shown here, when compared with measured waves, these observations appear to be quite reasonable.

CHESAPEAKE LIGHTSHIP

Three years (1/70-12/72) and a total of 3917 wave observations are available on magnetic tape from N.O.A.A. Environmental Data Service (Asheville, N.C.) for the Chesapeake Lightship. The lightship is located in forty feet of water off the entrance to

the Chesapeake Bay. Data is collected in the same manner as outlined above for the ship observation program and therefore the same limitations and errors associated with this program apply to the Chesapeake Lightship wave data (see Table 1).

The Chesapeake Lightship data is of value because it provides a wave climatology for inner shelf water depths, between the near shore and the deep water wave observation programs.

SMB HINDCAST DATA FOR CHESAPEAKE BAY ENTRANCE

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26,260 wave observations for Chespeake Bay Lightship position were hindcasted with the Bretschneider revised Sverdrup-Munk's method using U.S. Weather Bureau maps for the three year period 1948-1950 by Thorndike Saville, Jr., of the Beach Erosion board (Saville, 1954). Fetch and wind ' speed and direction were determined from North America Surface Synoptic charts at six hour intervals. Significant wave heights and periods were computed using the SMB method and compiled by height, period, and direction on a monthly and yearly basis.

The SMB is a simple empirical model for hindcasting deep water significant waves. Shallow water wave parameters must be determined by using wave refraction across the shelf. Results from such a simple model must be applied with caution (see Table 1). The SMB method is useful to the coastal engineer because wave parameters, especially for extreme wave

events, can be determined with a minimum of time and data. However, their results do not always agree with other data (Goldsmith, et al., 1974).

VIRGINIA BEACH WAVE GAGE

Of all the data presented in this report those from the wave gage should be considered the most reliable. A step resistance gage operated by the Coastal Engineering Research Center (U.S. Army Corps of Engineers) between 1/64-10/69 was located on the 15th street fishing pier in 20 feet of water. Due to repairs, instrument failure, and natural and unnatural destruction some months are missing from the 5½ year record. Summaries for the Virginia Beach Gage which indicate the months the gage was operative, are included in the appendix to this report.

A step resistance gage uses electrical contact points along a staff to sense water surface elevation. It appears (Esteva and Harris, 1970) that the SR gage estimates wave heights 20% greater than other gage types for high waves and about one foot too high for low and moderate wave conditions. Run up inside the H-Beam that supports the gage and biological fouling appear to account for the higher estimates of wave height from a step resistance gage.

During the period of operation for the Virginia Beach gage CERC changed methods for recording and analysis of wave data. Between 1965-1968 pen and ink records were used while since

November, 1968 signals from the wave gage were sent automatically over telephone lines and converted to digital records. Only a brief outline of CERC procedures for analysis of pen and ink and digital wave records follow. A more detailed description can be found in Harris (1970) or Thompson and Harris (1975).

Wave period templates were used to estimate the period of the higher heights and more uniform waves from pen and ink records. By dividing the length of a record by the period, the number of waves in the record can be estimated. From this a semi-objective procedure is used, based on the assumption that wave heights conform to a Rayleigh distribution function, to determine the rank 'n' of a wave which theoretically will have a height equal to the significant wave height. The height of this 'n'th highest wave is measured and constitutes the observation of significant wave height for that six hour period.

After November, 1968, the Virginia Beach gage wave records were recorded digitally and analysed by computer. This analysis procedure uses a wave spectrum to determine the wave parameters. Since a wave record will contain individual waves of varying height and period, a wave spectrum better represents a field of waves. Based on the assumptions that the wave heights can conform to a Rayleigh distribution and that the sea is represented by a narrow

band of energy spectrum, the significant wave height has been defined as four times the standard deviation of the record. The significant wave period is defined as the period of maximum energy density for the computed energy spectrum.

A wave climatology determined from the Virginia Beach gage should be reliable within the limitations imposed by the wave gage (see Table 1) for nearshore coastal engineering design and planning; however, wave direction is not measured.

DATA PRESENTATION AND USAGE BY THE ENGINEER

This wave climate has been prepared from an unusually large and varied data base. Wherever possible the data from all sources is presented in a unified format. However, the following differences in methodology amongst the various programs hinders this effort:

a) Wave heights and periods are often grouped in different intervals and units. For example, COSOP wave heights are recorded in one foot intervals, the wave gage data in $\frac{1}{2}$ foot intervals and the ship observation data is listed in $1\frac{1}{2}$ meter intervals.

b) Periods of sampling differ (Figure 2).

c) Methods of observation differ.

d) Virginia Beach gage lacks wave direction data.

e) Directional data is recorded in both 8 (COSOP) and 12 point (Ship Observations, Chesapeake Lightship, SMB calculations) compass directions.

The reader is advised to keep these differences in mind while reviewing the data presented in the following figures and tables.

TABLES

Table 1 lists errors and limitations associated with each data source.

Tables 2-5 are summaries for each directional data source of significant wave height and direction expressed

as percent of observations for the entire length of record. Direction refers to the compass points <u>from which</u> the waves approach. Height and direction intervals vary among the tables.

Table 6 is a summary of significant wave height and period for forty-five months of Virginia Beach wave gage data expressed as percent of total observations. This compilation represents a summary of both pen and ink and digital (see methods section) data. No calm conditions (CERC procedure) are included in this summary.

Tables 7 and 8 list the average $(\Sigma x/n)$ seasonal significant wave heights (meters) and periods (seconds) for each season. Winter is considered December-March; Spring is considered April-May; Summer is June-September; and Fall is October-November. N.O.A.A. Environmental Data Service (which provided most of the data) uses this particular grouping; therefore, in an effort to standardize format of presentation, all data has been grouped this way. As discussed later in the section on seasonality, this may not be the best possible format for this area.

The \pm standard deviation of each average H_s and T_s , a measure of the dispersion of individual observations about the mean value is presented as

 $\sigma = \sqrt{\frac{\sum x^2 - (\sum x)^2/n}{n-1}}.$

20

Tables 9-12 list seasonal average percentages of wave height by direction expressed as percent of total observations. The last row for each season lists the percent of waves from each direction greater than, or equal to, either five feet (SMB and COSOP data) or three meters (ship observations and Chesapeake Light). This value is simply the sum of each direction column for waves above three meters or five feet.

Table 13 lists the duration in hours of waves in the entire Virginia Beach gage record which exceeded a significant wave height of nine feet. Only the months during which these highest waves occurred are listed. For each of the three significant wave heights (9.5', 10.5', and 11.5'), there are listed the computations corresponding to $H_{1/10}$ (the average of the highest 10% waves), and H_{max} (the highest anticipated wave height). Most wave records are expressed in significant wave height. Therefore, parameters such as $H_{1/10}$ and H_{max} must be calculated based on the assumption that wave heights conform to the Rayleigh distribution. $H_{1/10}$ and H_{max} are calculated according to the relations; $H_{1/10} = 1.28$ H_s and $H_{max} = 1.77$ H_s, after Longuet-Higgins (1952).

For the Virginia Beach gage, each of the measurements are made every six hours and is considered statistically representative of a duration of six hours. In order to determine the duration in hours for each listed wave height, the percent of observations for the given height was multiplied by six and by the total number of observations.

Table 14 lists the tropical and extratropical storms which occurred during the period of record for the Virginia The term storm (extratropical) was defined by Beach gage. Richardson (personal communication) as having a storm surge of two feet or greater at a tidal gage, which in this area, was at Hampton Roads, Virginia. The Virginia Beach wave gage record is missing during only two of these storms, one of which occurred five days following another storm which had destroyed the gage. Wind speeds and directions are from the Norfolk Weather Station located at the Norfolk Regional The speed associated with each storm represents the Airport. highest wind (m.p.h.) that lasted for over one minute, during The wave heights associated with each storm from the storm. the Virginia Beach gage are then listed. Again as in Table 13, $H_{1/10}$ and H_{max} are calculated values (after Longuet-Higgins, 1952).

Tropical storm data is compiled identically as for extratropical storms except that storm names are also listed.

Table 15 is a compilation of wave refraction data available from the VIMS-VSWCM (Virginia Sea Wave Climate Model) data bank (Goldsmith, et al., 1974). The data summarizes changes in deep water waves ($H_0 = 6$ feet) as they cross the shelf between 30 and 20 feet of water for eight and ten second waves from the Northeast, East, and Southeast. Wave height for six to ten wave rays (see Figures 14-20) refracting into

shore between Dam Neck and Virginia Beach were averaged* in about 20 and 30 feet of water.

In general, Dam Neck is an area of relatively low wave energy from the northeast waves (due to extensive refraction by the Virginia Beach Massif), and is an area of wave energy concentration for southeast, and to a lesser extent east, waves (see discussion in Goldsmith, et al., 1974, p. 37).

Table 16 represents a compilation of the daily VIMS-CERC volunteer wave observer data organized according to location (between Virginia Beach, Virginia and Currituck Beach Light, North Carolina) and by season. It appears that the greatest wave heights occur in the summer months while the longest wave periods seem to occur during the fall. However, the data varies widely between observers (especially wave periods), and the seasonal differences for most observers are probably statistically non-significant. Thus, because of all the problems involved in data from untrained wave observers and irregular data collection, little credence should be given these wave data.

*An average height is used because the depth grid (0.5 nm) employed in the Virginian Sea Wave Climate Model is too coarse to be site specific for the proposed outfall site, and computations from a single ray could be misleading.

FIGURES

Figures 1a & 1b & 1c are maps showing the location of data sources and the proposed sewage outfall.

Figure 1d is a diagram which shows the percent of total number of waves in each wave height range and the location of H_s ($H_{1/3}$) and $H_{1/10}$ on the distribution.

Figure 2 compares the lengths and dates of records, and presents the number of observations, measurements or computations for each data source.

Figure 3 is a graphical comparison of the average significant wave heights for each data source, by season, which are listed in Table 7.

Figure 4 is a graphical comparison of the average significant periods for each data source, by season, which are listed in Table 8.

Figure 5 is a representation of monthly and seasonal significant wave heights (see Table 7 and Appendix) for the Virginia Beach gage. An envelope of one standard deviation which represents the dispersion of individual waves about the average monthly significant wave height is also represented in this figure. 68% of all waves for a given month have occurred within an envelope represented by + and - one standard deviation value.

Figure 6 is identical to Figure 5 except that it represents the significant wave period.

Figure 7 represents the frequency (expressed in percent of total observations) with which waves higher than a given height have occurred during the period of record. Cumulative frequencies, with the 100% level set at waves greater than or equal to zero feet, are constructed from Tables 1-6, and then plotted on semi-log paper with these data points clearly shown. In following the curves to extreme heights (low frequencies), it should be remembered that the lines are visually extrapolated and that data exists only for the points indicated.

From this Figure and Figure 2 the frequency of occurrence in number/year of a particular significant wave height can be estimated. For example, from the COSOP curve it is seen that a wave height of 10 feet or greater occurred only .02% of the time during 4/54-12/65. Therefore, there are only .0002 x 25,338 total observations or five wave observations over a height of ten feet. Since each observation is considered to represent four hours of record there were a total of 4 x 5 or 20 hours of waves over ten feet between 4/54-12/65. Since this is 20/24 of a day and there are (25,338/6) days in the record, then wave heights above ten feet for the COSOP data occurred once in (20/24)/(25,338/6) = .83/4223 days or one day in 14.36 years, or one observation per 2.36 years.

Figure 8 for the Virginia Beach gage is similar to Figure 6 but it also shows a curve calculated for $H_{1/10}$ from H_s . An example below demonstrates calculation in number/year of waves with $H_s \ge 11$ feet, or $H_{1/10} \ge 14$ feet.

25,

 $H_s \ge 11$ feet occurs = .05% Total # of observations = 6354 # of observations ≥ 11 feet = 3.18 Duration ≥ 11 feet = 3.18 x 6 = 19.08 hours (19.08)//635

Number of days per year $=\left(\frac{19.08}{24}\right) \left| \left(\frac{6354.}{4}\right) \right|$ H_s > 11 feet, H_{1/10} > 14 feet = 1 day/5.4 years = 3.18 obs./1558 day

= 1 observation/1.35 years

Figures 9-14 are wave roses showing pictorially the percentage occurrence of waves of different height from each direction. The data is listed in Tables 2-5 and 9. Differences in rose format are necessary due to methods and categories of data collection. All waves from between 195°-345° azimuth (0° is north) are neglected because the shoreline of interest in this report is oriented about north-south. The COSOP data is further reduced to seasonal wave roses (Table 9) to evaluate changes in nearshore direction of wave height and approach.

Figure 15-20 (from Goldsmith, et al., 1974) are wave ray diagrams for 6 wave conditions in the VIMS-NASA-LANGLEY Virginia Sea Wave Climate Model. Wave rays approaching the shoreline between Dam Neck and Virginia Beach were selected for the compilation of data in Table 15.

DISCUSSION

VARIATIONS ACROSS THE ADJACENT CONTINENTAL SHELF

This wave climate synthesis represents data derived from surf, shallow water, mid-water, and deep water wave conditions. As waves travel across this very wide and high relief shelf into shallow water they are primarily affected by refraction, shoaling and bottom friction. Due to these effects, monitoring stations should detect at least two general changes in wave characteristics for waves traveling from deep to shallow water: 1) The angle of wave approach relative to the shoreline should progressively reduce (wave crests become increasingly parallel to the coast). 2) Wave heights will greatly decrease from friction, and either decrease or increase from refraction. Given all of the variability, unreliability, nonuniform sampling periods, and a large error associated with wave observers, it is completely surprising, but very gratifying to note that comparisons of wave sources which reflect different depths along the shelf actually do indicate these changes in wave characteristics (Tables 7, 8 and Figures 3, 7).

Wave Height

The following conclusions, regarding changes in wave height distributions across the shelf in the Virginia Beach Area, were arrived at from comparisons of the various data presented in this report.

1) Deep water average significant wave heights are generally about two feet higher (SMB Hindcast, Chesapeake Lightship and Ship Observations) than the averages for shallow water conditions (COSOP and Virginia Beach Gage).

2) The largest average significant wave (see Figure 3) heights are associated with the hindcast data. Note also (see Tables 2-5) that the percent greater than or equal to 10 feet (~ 3 meters) is 6.8 for SMB hindcast while only 2.1% for ship and 1.4% for the Chesapeake Lightship observations. These higher averages would be expected because of the simple assumptions of the SMB computations, the avoidance of extreme conditions by ships, and the evacuation of the lightship during extreme wave events, and the fact that only the SMB hindcasted wave observations are for strictly deep water conditions, since the Ship Wave Observations encompassed within the 1° square contain an unknown amount of wave data taken in depths less than "deep" water for the longer period waves.

3) Ship observations in MS 116, SS-65 do not represent only deep water conditions, but instead a range of depths from deep to shallow. Due to this range, the average wave heights from ship data might be expected to conform to more mid-shelf conditions. The Chesapeake Lightship is anchored in the innershelf (40 feet) and it is interesting to note that average significant wave heights for both sources are essentially the same, though winter values are higher and summer values lower for the ship observations.

4) Since larger wave heights are associated with breaking waves (which are monitored by the shoreline COSOP program) than with nonbreaking waves, it is not surprising that average significant wave heights are slightly higher for the COSOP data than the wave gage, even though the gage is located in 20 foot water depths.

5) The frequency of occurrence of waves greater than a given height is, as would be expected, higher on the shelf than in nearshore water (see Figure 7). For example, waves greater than or equal to 10 feet had a frequency occurrence of only .2% in 20 feet of water (Virginia Beach gage), but 2% in 40 feet of water (Chesapeake Lightship) and 7% in deep water (SMB hindcast). The frequency occurrence of waves greater than about five feet is slightly higher for the Virginia Beach gage than COSOP data. This difference is likely due to unequal sampling periods, that is the five years of gage record was unusually stormy compared to the 20 years of COSOP record. In addition, COSOP observations often do not include extreme wave events while the gage does. Also, note the high standard deviations of both data sets in Table 7.

Wave Period

Analysis of wave period data receives little emphasis in this report because large differences in average wave periods exist between the data sources, differences which are not induced by waves traveling across the shelf but due to differ-

ences in methodology and observer errors. For example, over 99% of all observations from the Chesapeake Lightship recorded wave periods of five seconds and less, which probably indicates bias and error due to the observers and recording procedure, and not a dominance of 5 second waves. From Table 8, it is seen that the average significant wave periods range from five to ten seconds with no relation to depth induced changes. The only objective wave period information of use to the coastal engineer is available from wave gage records. This information is supplied in Table 6.

There is, however, one trend apparent in Table 8, which explains the weaknesses in these data. The measured (Virginia Beach Gage) and computed waves (SMB) have the highest wave periods, approximately 8 to 10 seconds, respectively, for all seasons; whereas all other data (observed) is about 5 seconds. This is because when two superimposed wave trains occur, even the trained observer generally sees only the shorter period waves. In this area it is very common to have a local "sea" combined with a longer period swell produced by a distant storm. Evidently, most observers see only the local sea. Thus, only data measured by instruments, and statistically processed, will show the correct percentage of longer period waves.

Wave Direction

The anticipated changes in direction of approach of waves traveling across the shelf are well documented in this report. The dominant angle of approach relative to the shoreline,

decreases for monitoring stations in increasingly shallow water. Comparison of COSOP, Ship, and Chesapeake Lightship Observations show for increasingly nearshore conditions diminishing northerly and southerly components (wave crests perpendicular to shore) and increasing easterly components (wave crests parallel to shore).

SEASONALITY

Information regarding seasonal changes in wave characteristics is important to coastal engineers trying to most efficiently and safely plan the use of construction vessels. The data presented in this report indicates changes, though small, in seasonal wave characteristics. According to Hayden (1975) annual cycles of wave climate exist along the east coast of the United States. For the Virginia Beach area, Hayden (1975) found a winter to summer transition data of April 10, and a summer to winter transition at August 17, based on the same COSOP data presented in this report.

Wave Height

Figure 3 examines the seasonality of significant wave height for all wave sources. It is evident that these seasonal height averages are greater during the winter and fall, and lower during the spring and summer. The differences between summer and winter averages range from as little as .1 foot for the COSOP data to 1.4 feet for the ship data. In any case, considering the large standard deviations, (Table 7) most differences are probably not important.

Figure 4 is an analysis of monthly data for the Virginia Beach gage, which is of most use, and the most reliable for nearshore coastal engineering. It is evident that the highest significant average heights occur between September-October and December-March with the lowest between April-August. Given a standard deviation (dashed line) of about 1.5 feet, this average seasonal difference of .4 feet between summer and winter should be regarded as being unimportant. Although there is a slightly higher probability of 4 foot waves during the winter than summer at Virginia Beach, it should be noted that 68% (± 1st deviation) of all waves during all months had significant wave heights less than 4.2 feet ($H_{1/10} = 5.1$ foot). From Table 13 it is seen that 99.7% of all waves during all months were less than H_s of 9.5 feet ($H_{1/10}$ of 12.2 foot). If $H_s = 9.5$ feet is of no concern to the coastal engineer, than seasonality should be of no concern. However, twice as many waves over 5 feet occurred between December and March (5.4%) than between April-August (2.2%), though in either case, the total number was small.

Figure 3 also compares seasonal and monthly average significant wave heights. The data clearly shows that the use by NOAA (see discussion of Tables 7 & 8) of seasonal groupings which include September as a summer month is not a good practice for this area. September average significant wave heights are as large as those for the winter months. This conclusion confirms Hayden's data of winter to summer transition during August.

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Wave Direction

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The direction of wave approach changes between winter and summer months. Figures 10 & 11, depicting data presented in Table 9, show the predominance of Southeast and Easterly components during the summer, and Northeast and Easterly components during the winter for nearshore wave conditions (COSOP data).

REPRESENTATIVENESS OF VIRGINIA BEACH GAGE WAVE DATA

For nearshore coastal engineering design and planning, a wave gage supplies the most reliable and objective wave climatology available. However, application of these gage data is limited by two critical issues: 1) The period of record for the gage (4/64-10/69) may not represent typical wave conditions, but instead abnormally calm or stormy periods; 2) The location and depth of the gage may not reflect conditions at the exact location of the proposed structure. These problems are discussed below.

1) As noted in the first section describing the design of the Virginia Beach gage, data from a step resistant gage is a conservative estimate of wave height distributions.

2) Data collected by W.S. Richardson at Techniques Development Lab of the U.S. Weather Service between 1957-1969 indicate that there were an average of three extratropical storms per year. Table 14 lists the occurrence of tropical and extratropical storms during the period of operation of the Virginia Beach gage. There were 16 extratropical storms over

a five year period, or an average of 3 storms/year. There were also a number of intense storms during the same period (e.g., 1/16/65, 11/9/68, 3/1/69).

3) Table 14 also lists tropical storms during the period of record of the gage from data compiled by the Norfolk Weather Station. The storms listed do not represent the most intense hurricanes of the century, but only extratropical events of average intensity.

4) Comparisons such as Figures 3 & 7 demonstrate that the average significant wave heights from the wave gage data fit well into the range of values expected due to waves crossing the shelf.

5) a. Table 15 summarizes the data available in the VIMS Virginian Sea Wave Climate Model Data Bank (Goldsmith, et al., 1974) of the changes in wave height due to refraction, shoaling and friction between deep water and depths of 30 to 20 feet for a variety of wave directions and periods. The data presented is for an average of 6 to 10 rays reaching the Virginia Beach to Dam Neck area. From Table 15 it is seen that these wave heights change an average of only .1 foot between a depth of 20 and 30 feet while passing over this shelf area.

b. The alongshore variation in wave heights between6 to 10 wave rays is negligible.

6) Except for a very limited number of waves the gage located in 20 feet of water measures only nonbreaking waves (see following section).

From the above discussion it can be concluded that fortyfive months of data recorded by a gage located in 20 feet of water at Virginia Beach is directly applicable to conditions at Dam Neck in 30 feet of water at the proposed depth of the diffuser section, subject to <u>detailed</u> wave refraction studies.

EXTREME WAVE CLIMATE

The magnitude and frequency of occurrence of extreme wave events determine the design of many marine structures. Nearshore wave gages provide the most reliable recorded data for construction of extreme wave climates. Tables 13 & 14, and Figure 7 & 8 summarize the most pertinent extreme wave data.

The highest significant wave height (H_s) which occurred during the entire period of record of the Virginia Beach was 11.5 feet. However, given the definition of H_s we know that waves above 11.5 feet occurred. During the 19 hours of measured H_s = 11.5 feet a number of waves up to 14.7 feet (H_{1/10}) and a very small number of waves up to 20.4 feet (H_{max}) could be expected. During the entire record of the gage the highest wave likely to have occurred was 20.4 feet, but only very few (less than ten) isolated waves would reach this height.

It is of interest to the coastal engineer whether or not waves will be breaking over the proposed structure. Munk (1949) established the relation:

$$\frac{b}{H} = 1.28$$

where $D_b =$ water depth at breaking where $H_b =$ water height at breaking

This relation provides a rough idea of the limiting height or depth of breaking waves. No recorded H_s or H_{1/10} would have broken at the gage while the H_{max} recorded was probably just beginning to break. A storm condition with 20 foot waves might be expected to be accompanied by a storm surge of several feet which at high tide could increase the water depth at the gage to 26 feet. Thus, the rare H_{max} of 20.4 feet would just break at this 26 foot depth. Therefore, the Virginia Beach gage recorded exclusively nonbreaking waves, with only a few exceptions (less than 10).

On the other hand in 30 feet of water, the depth of the proposed diffuser, (or 36 feet in a severe storm) no waves which were recorded by the Virginia Beach gage would have been breaking waves.

The extreme wave climate presented in this report is limited by the length of record. Between 1964 and 1969 no waves of H_s over 11.5 feet were observed. This does not necessarily mean that no waves with higher significant wave heights will occur at the proposed site. For example, a significant wave height greater than 11.5 feet might have occurred during the 1962 Ash Wednesday storm, the 100 year storm. Anticipated wave heights for such a storm could be estimated using wave hindcasting and refraction techniques.

However, extrapolation of Figure 8 to low frequencies of occurrence seems justifiable from the comparison of the Virginia Beach gage curve with longer record curves such as the ship data. Extrapolated to the .01 percent level, a wave height $H_s = 13.5$, $H_{1/10} = 17.28$ and a $H_{max} = 23.9$ feet might be expected to occur one day in 27 years. Therefore this extrapolated wave height distribution might be a better estimate of the extreme wave height that is likely to occur in the Virginia Beach Dam Neck area than the shorter period measured waves. The fact that the gage design itself promotes conservative height estimates supports this conclusion.

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WAVE SOURCES

COAST GUARD-CERC COOPERATIVE SURF OBSERVATION PROGRAM at Virginia Beach C. G. Station

ERRORS & LIMITATIONS

- Surf zone conditions only 1)
- 2) Waves fully affected by: Refraction a.
 - Bottom friction Ъ.
 - c. Wave breaking
- 3) Site specific with respect to longshore variations of wave energy
- Data often lacking for 4) extreme events (CERC. 1973)
- 5) Observer bias and errors
- 6) Observations at unknown tidal stage

APPLICATION SITE SPECIFIC AND SHOULD NOT BE USED FOR SPECIFIC STRUCTURAL DESIGN

VIMS-CERC VOLUNTARY WAVE **OBSERVER PROGRAM at 10** Locations along the Coast

- 1) Surf zone conditions only
- 2) Waves fully affected by:
 - a. Refraction
 - Bottom friction Ъ.
 - c. Wave breaking
- Data usually lacking for 3) extreme events
- 4) Observer bias and errors
- 5) Short duration of record
- 6) One observation per day and 5/week
- 7) Untrained observers
- Many sites along coast 8)
- 9) Observations at unknown tidal stage

APPLICATION ONLY TO ESTIMATE LONGSHORE VARIATION OF WAVE ENERGY

VIRGINIA BEACH WAVE GAGE

- Nearshore conditions 1) 2)
 - Wave affected by:
 - a. Refraction
 - Bottom friction Ъ.
 - Non-directional record
- 4) Overestimate of height due to gage type
- 5) Incomplete record
- Two methods of recording and 6) analyses
- Site specific 7)

3)

MOST RELIABLE AND PRECISE INFORMATION SEA-WARD OF BREAKERS UNDER ALL CONDITIONS FOR NEARSHORE DESIGN AND PLANNING PROBLEMS

Table 1. (cont.)

WAVE SOURCES

OBSERVATIONS

CHESAPEAKE LIGHTSHIP

ERRORS & LIMITATIONS

- 1) Inner shelf (40 ft. depths) conditions
- Ambiguity and errors with coding of data
- 3) Unreliable wave observers4) Evacuated during extreme
- 4) Evacuated during extreme events

5) Short duration of record PROVIDES A WAVE CLIMATOLOGY, ALTHOUGH NOT PRECISE FOR MIDDEPTH CONDITIONS

SHIPBOARD WAVE OBSERVATIONS

- 1) Deep water conditions
- 2) Data grouped from many locations and depths
- 3) Ambiguity and errors due to coding of data
- 4) Unreliable, untrained wave observers
- 5) Ships avoid extreme wave events

PROVIDES A WAVE CLIMATOLOGY, ALTHOUGH NOT PRECISE FOR DEEP WATER CONDITIONS

SMB HINDCAST COMPUTATIONS

- Assume deep water conditions 360° around site
- 2) Simple model used to generate the wave parameters
- 3) Short period of record
- 4) Changing metereological conditions since sample period (1948-1950)
- 5) Appears to give highest % of larger wave heights, and therefore may be biased towards extreme events

PROVIDES A SIMPLE, ALTHOUGH NOT PRECISE ESTIMATE OF WAVE CONDITIONS FOR DEEP WATER

Table 2.

COSOP 4/54-12/65

Average Percentages for Significant Wave Heights (rows) by Direction (columns)

	North	NE	East	SE	South	SW	West	NW	Total
0-1	.00	.02	.16	,06	.00	.00	.00	.00	.24
1-2	.02	5.04	18.72	12.79	,00	.00	.00	.00	36.58
2-3	.01	8.80	17.70	13,99	.03	.00	.00	.00	40.53
3-4	.00	6.34	5.77	3.98	.00	.00	,00	.00	16.10
4-5	.00	2.51	1.26	.64	.00	.00	.00	.00	4.41
5-6	.00	.91	.41	.09	.00	.00	.00	.00	1.41
6-7	.01	.34	.18	,08	.00	.00	.00	.00	.60
7-8	.00	.03	.02	.03	, 00	.00	.00	.00	.07
8-9	.00	.02	.00	.02	.00	,00	.00	.00	.04
9-10	.00	,00	.00	.00	.00	.00	.00	.00	.00
10+	.00	.00	.01	.00	.00	.00	.00	.00	.02
[otal	.04	24.00	44.23	31.68	.04	.01	.00	٥٥ ،	100.00 100.00
% ≥ 5	.01	1.30	.61	.22	0	0	0	0	2.14

Table 3.

CHESAPEAKE LIGHTSHIP 1/70-12/72

Average Percentages for Significant Wave Heights (rows) by Direction (columns)

		<u>345°-15°</u>	<u>15°-45°</u>	<u>45°-75°</u>	<u>75°-105°</u>	<u>105°-135°</u>	<u>135°-165°</u>	<u>165°-195°</u>	<u>Total</u>
	< 1	2.18	4.23	3.25	3.73	5.2	5.93	4.85	29.37
	1-1.5	3.85	7.7	6.38	7,93	6.78	7.58	3.95	44.17
•	2-2.5	.31	1.3	1.28	. 75	.6	.38	.38	5.0
	3-3.5	.1	.58	.15	.33	.03	.05	.05	1,29
	4-5.5	.05	0	0	.03	.03	0,	0	.11
	6-7.5	0	0	0	0	0	0	0	0
	8-9.5	0	0	0.	0	0	0	0	0
2 1.	> 9.5	0	0	0	0	0	0	0	0
	Total	6.485	13.08	11.05	12.75	12.63	13.93	9.23	79,94
% ≥ 3	3 meters	.15	.58	.15	.36	.06	.05	.05	1.40

Table 4.

SHIP OBSERVATIONS 12/48-12/72

Average Percentages for Significant Wave Heights (rows) by Direction (columns)

	<u>345°-15°</u>	<u>15°-45°</u>	<u>45°-75°</u>	<u>75°-105°</u>	<u>105°-135°</u>	<u>135°-165°</u>	<u>165°-195°</u>	<u>Total</u>
< 1	2.78	2.98	3.25	3.03	2,48	4.23	4,48	23.23
1-1.5	4.7	3.8	4.96	4.03	2.48	4.03	3.83	27.83
2-2,5	1.23	1.2	1.2	.5	.35	.43	.53	5.44
3-3.5	.35	.4	.33	.18	.04	.13	.1	1,53
4-5.5	.06	.1	.21	.06	.03	0	.05	.5
6-7.5	0	.06	.01	0	0	0	0	.07
8-9.5	0	.01	.01	0	0	0	0	.02
> 9.5	0	0	0	0	0	0	0	0
Total	9.12	8.55	9.97	7.8	5.38	8.82	8.99	58.62
$\% \ge 3$ meters	.41	.5	.54	.24	.07	.13	.15	2.1

Table 5.

SMB HINDCAST 1/48-12/50

Average Percentages for Significant Wave Heights (rows) by Direction (columns)

	North	NNE	NE	ENE	East	ESE	SE	SSE	South	<u>Total</u>
.5- 2	0	0	8.16	17.66	8.57	1.93	1.31	.65	.46	38.74
2- 4	0	.03	5.83	12.94	5.10	1.71	1.23	.70	.62	28.16
4- 6	0	.12	2.86	7.28	2.34	1.03	.73	.35	.14	14,85
6-8	.01	0	2.05	3.50	1.11	.44	.34	.23	.14	7.91
8-10	0	.13	1.12	1.40	.72	.35	.34	.11	.09	4.26
10-12	0	0	, 62	.73	.40	.08	.20	.11	.10	2.24
12-14	0	.12	.62	.43	.15	.18	.11	0	.03	1.64
14-16	0	0	.37	.34	.05	.06	.05	.02	0	.89
16-18	0	.01	.20	.11	.03	.03	.02	0	.02	.42
18-20	0	0	.14	.11	.05	.02	.02	0	0	.32
20-25	0	.02	.15	.15	.05	0	.02	.05	0	.44
25-30	0	.01	.04	.09	0	0	0	0	0	.14
Total	.01	.44	21.16	44.74	18.53	5.83	4.37	2.22	1.6	100.01
10 feet	0	.16	2.4	5.8	.69	.37	.42	.18	.15	10.17

.% ≥

Table 6.

VIRGINIA BEACH GAGE 4/64-10/69

Average Percentages of Significant Height (columns) versus Period (rows)

0-1,0 <		0-1	<u>1-2</u>	<u>2-3</u>	<u>3-4</u>	4-5	5-6	6-7	<u>7-8</u>	<u>8-9</u>	9-10	<u>10-11</u>	<u>11-12</u>	<u>Total</u>
2.0-2.9 .03 .15 .08 0 <	0- 1.0	0	0	0	0	0	0	0	0	0	0	0	0	0
3.0-3.9 .53 2.68 .94 .13 0 0 0 0 0 0 0 0 0 0 3.9 4.0-4.9 .30 2.10 2.35 .83 .25 .11 0 <td>2.0- 2.9</td> <td>.03</td> <td>.15</td> <td>.08</td> <td>0</td> <td>0</td> <td>0</td> <td>0</td> <td>0</td> <td>0</td> <td>0</td> <td>0</td> <td>0</td> <td>.21</td>	2.0- 2.9	.03	.15	.08	0	0	0	0	0	0	0	0	0	.21
4.0-4.9 .30 2.10 2.35 .83 .25 .11 0 0 0 0 0 0 0 0 9.4 5.0-5.9 .38 3.21 3.66 1.61 .58 .38 .03 0 0 0 0 0 9.4 6.0-6.9 .53 4.22 2.38 1.09 .81 .56 .28 .08 0 0 0 9.4 7.0-7.9 1.06 5.64 2.43 .78 .48 .38 .28 .18 .11 0 0 0 10.2 8.0-8.9 1.97 10.56 5.38 .73 .45 .23 .11 .11 .13 .15 .08 .10 18.0 9.0-9.9 1.06 9.88 2.68 .58 .20 .15 .11 0 .15 .08 .10 18.0 10.0-10.9 1.21 5.33 2.27 .56 .28 .01 .15 .03 .03 .03 0 0 .47 13.0-13.9<	3.0- 3.9	.53	2.68	.94	.13	0	0	0	0	0	0	0	0	3.92
5.0-5.9 .38 3.21 3.66 1.61 .58 .38 .03 0 0 0 0 9.4 6.0-6.9 .53 4.22 2.38 1.09 .81 .56 .28 .08 0 0 0 9.4 7.0-7.9 1.06 5.64 2.43 .78 .48 .38 .28 .18 .11 0 0 0 10.2 8.0-8.9 1.97 10.56 5.38 .73 .45 .23 .11 .11 .13 .15 .08 .10 18.0 9.0-9.9 1.06 9.88 2.68 .58 .20 .15 .11 0 .15 .08 .10 13.7 10.0-10.9 1.21 5.33 2.27 .56 .28 .01 .15 .03 .03 .03 0 0 0 .7 11.0-11.9 .53 2.58 .99 .30 .08 0 0 0 0 0 .17 13.0-13.9 .15 .76 .30 <t< td=""><td>4.0- 4.9</td><td>.30</td><td>2.10</td><td>2.35</td><td>.83</td><td>,25</td><td>.11</td><td>0</td><td>0</td><td>0</td><td>0</td><td>0</td><td>0</td><td>5.63</td></t<>	4.0- 4.9	.30	2.10	2.35	.83	,25	.11	0	0	0	0	0	0	5.63
6.0-6.9 .53 4.22 2.38 1.09 .81 .56 .28 .08 0 0 0 9.4 7.0-7.9 1.06 5.64 2.43 .78 .48 .38 .28 .18 .11 0 0 0 10.2 8.0-8.9 1.97 10.56 5.38 .73 .45 .23 .11 .11 .13 .15 .08 .10 18.0 9.0-9.9 1.06 9.88 2.68 .58 .20 .15 .11 0 .15 0 0 0 13.7 10.0-10.9 1.21 5.33 2.27 .56 .28 .01 .15 .03 .03 .03 0 8.7 11.0-11.9 .53 2.58 .99 .30 .08 0 0 0 0 0 3.9 12.0-12.9 .51 2.30 1.04 .91 .28 .13 .13 0 0 0 0 1.47 13.0-13.9 .15 .76 .30 .15 <	5.0- 5.9	.38	3.21	3.66	1.61	,58	.38	.03	_0	0	0	0	0	9.47
7.0-7.9 1.06 5.64 2.43 .78 .48 .38 .28 .18 .11 0 0 10.2 8.0-8.9 1.97 10.56 5.38 .73 .45 .23 .11 .11 .13 .15 .08 .10 18.0 9.0-9.9 1.06 9.88 2.68 .58 .20 .15 .11 0 .15 0 0 13.7 10.0-10.9 1.21 5.33 2.27 .56 .28 .01 .15 .03 .03 .03 0 0 8.7 11.0-11.9 .53 2.58 .99 .30 .08 0 0 0 0 0 3.9 12.0-12.9 .51 2.30 1.04 .91 .28 .13 .13 0 0 0 0 4.7 13.0-13.9 .15 .76 .30 .15 .08 .08 0 0 0 0 1.9 15.0-15.9 .08 .08 0 0 0 0 0	6.0- 6.9	,53	4.22	2.38	1.09	.81	.56	,28	.08	0	0	0	0	9.42
8.0-8.9 1.97 10.56 5.38 .73 .45 .23 .11 .11 .13 .15 .08 .10 18.0 9.0-9.9 1.06 9.88 2.68 .58 .20 .15 .11 0 .15 0 0 0 13.7 10.0-10.9 1.21 5.33 2.27 .56 .28 .01 .15 .03 .03 .03 0 0 8.7 11.0-11.9 .53 2.58 .99 .30 .08 0 0 0 0 0 3.9 12.0-12.9 .51 2.30 1.04 .91 .28 .13 .13 0 0 0 0 4.7 13.0-13.9 .15 .76 .30 .15 .08 .08 0 0 0 0 0 1.9 15.0-15.9 .08 .08 0 0 0 0 0 0 .10 .10 .10 16.0-16.9 0 .11 .05 0 0 0 0<	7.0- 7.9	1.06	5.64	2.43	.78	.48	,38	.28	.18	.11	0	0	0	10.28
9.0-9.9 1.06 9.88 2.68 .58 .20 .15 .11 0 .15 0 0 0 13.7 10.0-10.9 1.21 5.33 2.27 .56 .28 .01 .15 .03 .03 .03 0 0 8.7 11.0-11.9 .53 2.58 .99 .30 .08 0 0 0 0 0 0 3.9 12.0-12.9 .51 2.30 1.04 .91 .28 .13 .13 0 0 0 0 4.7 13.0-13.9 .15 .76 .30 .15 .08 .08 0 0 0 0 1.3 14.0-14.9 .18 .71 .58 .25 .18 .18 .03 .03 0 0 0 1.9 15.0-15.9 .08 .08 0 0 0 0 0 0 0 0 0 0 0 0 0 1.9 16.0-16.9 0 .11 .05	8.0- 8.9	1.97	10.56	5.38	.73	,45	.23	.11	.11	.13	.15	.08	.10	18.03
10.0-10.9 1.21 5.33 2.27 .56 .28 .01 .15 .03 .03 .03 0 0 8.7 11.0-11.9 .53 2.58 .99 .30 .08 0 0 0 0 0 0 3.9 12.0-12.9 .51 2.30 1.04 .91 .28 .13 .13 0 0 0 0 4.7 13.0-13.9 .15 .76 .30 .15 .08 .08 0 0 0 0 0 1.3 14.0-14.9 .18 .71 .58 .25 .18 .18 .03 .03 0 0 0 1.9 15.0-15.9 .08 .08 0 0 0 0 0 0 .04	9.0- 9.9	1.06	9.88	2.68	.58	.20	.15	,11	0	.15	0	0	Q	13.75
11.0-11.9 .53 2.58 .99 .30 .08 0 0 0 0 0 0 0 0 0 3.9 12.0-12.9 .51 2.30 1.04 .91 .28 .13 .13 0 0 0 0 4.7 13.0-13.9 .15 .76 .30 .15 .08 .08 0 0 0 0 0 1.3 14.0-14.9 .18 .71 .58 .25 .18 .18 .03 .03 0 0 0 1.9 15.0-15.9 .08 .08 0	10.0-10.9	1.21	5.33	2.27	.56	.28	.01	.15	.03	.03	.03	0	0	8.79
12.0-12.9 .51 2.30 1.04 .91 .28 .13 .13 0 0 0 0 4.7 13.0-13.9 .15 .76 .30 .15 .08 .08 0 0 0 0 0 1.3 14.0-14.9 .18 .71 .58 .25 .18 .18 .03 .03 0 0 0 1.9 15.0-15.9 .08 .08 0 0 0 0 0 0 .04 .04 16.0-16.9 0 .11 .05 0 0 0 0 0 0 .04 .04 .16 .08 .10 100.04	11.0-11.9	.53	2.58	.99	.30	.08	0	0	0	0	0	0	0	3.95
13.0-13.9 .15 .76 .30 .15 .08 .08 0 0 0 0 0 1.3 14.0-14.9 .18 .71 .58 .25 .18 .18 .03 .03 0 0 0 1.9 15.0-15.9 .08 .08 0	12.0-12.9	.51	2.30	1.04	.91	,28	.13	.13	.0	0	0	0	0	4.79
14.0-14.9 .18 .71 .58 .25 .18 .18 .03 .03 0 0 0 1.9 15.0-15.9 .08 .08 0 </td <td>13.0-13.9</td> <td>,15</td> <td>.76</td> <td>.30</td> <td>.15</td> <td>.08</td> <td>.08</td> <td>0</td> <td>0</td> <td>0</td> <td>0</td> <td>0</td> <td>0</td> <td>1.37</td>	13.0-13.9	,15	.76	.30	.15	.08	.08	0	0	0	0	0	0	1.37
15.0-15.9 .08 .08 0 0 0 0 0 0 0 0 0 0 0 0 0 .0<	14.0-14.9	.18	.71	.58	.25	.18	.18	.03	.03	0	0	0	0	1.96
16.0-16.9 0 .11 .05 0 0 0 0 0 0 0 0 0 0 .11 Total 8.52 50.30 26.15 7.98 3.67 2.29 1.11 1.09 .41 .18 .08 .10 100.06	15.0-15.9	.08	.08	0	0	0	. 0	0	0	0	. 0	0	0	.08
Total 8.52 50.30 26.15 7.98 3.67 2.29 1.11 1.09 .41 .18 .08 .10 100.00	16.0-16.9	0	.11	.05	0	0	0	0	0	0	. 0	0	0	.16
	Total	8.52	50.30	26.15	7.98	3.67	2.29	1.11	1.09	.41	.18	.08	.10	100.00

Table	7	
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	$\frac{\text{SEASONAL AVERAGE SIGNIFICANT WAVE HEIGHT}{\text{IN METERS AND STANDARD DEVIATION}} (\sigma)$											
Source	H _s Winter	σ <u>Winter</u>	H _s Spring	σ Spring	H _s Summer	σ Summer	Hs Fall	о <u>Fall</u>	Years			
Ship Obser.	1.23	.85	1.12	.77	.80	.57	1.15	.76	12/48-12/73			
Ches. Light	1.10	.63	1.02	.57	.99	.54	1.24	.66	1/70-12/72			
SMB Hindcast	1.28	1.10	1.09	.90	1.11	.93	1.07	.94	1/48- 1/50			
COSOP	.76	.93	.71	.85	.73	.94	.79	1.03	4/54-12/65			
Va. Beach Gage	.70	1.43	.61	1.08	.58	1.15	.74	1.23	4/64-10/69			

Table 8.

	$\frac{\text{SEASONAL AVERAGE SIGNIFICANT WAVE PERIOD}{\text{AND STANDARD DEVIATION}} (\sigma)$												
Source	T _s Winter	σ Winter	T _S Spring	σ Spring	T _s Summer	o Summer	Ts <u>Fall</u>	б <u>Fall</u>	Years				
Ship Obser.	5.37	1.7	5.21	1.87	5.18	1.44	5,43	1.71	12/48-12/73				
Ches. Light	4.54	.51	4.52	.3	4,56	.54	4,50	.17	1/70-12/72				
SMB Hindcast	10.44	2.92	10,0	2.41	9.56	2.84	9.89	2.96	1/48- 1/50				
COSOP	5.9	.77	5,98	.64	6.01	.70	5,93	.78	4/54-10/65				
Va. Beach Gage	8.2	2.71	7.93	2.39	8.49	2.10	8.80	2.48	4/64-10/69				

CERC	-COAST GU	JARD COOPERA	TIVE SURF	OBSERVATION	PROGRAM	4/54-12/65	
		Averag Heights (r	e Percent ows) by D December	agés for Wav irection (co -March	e lumns)		
	North	<u>N. East</u>	East	<u>S. East</u>	South	S. West	<u>Total</u>
$\begin{array}{c} 0-1\\ 1-2\\ 2-3\\ 3-4\\ 4-5\\ 5-6\\ 6-7\\ 7-8\\ 8-9\\ 9-10\\ 10+ \end{array}$	0 .1 .06 0 .05 0 0 0 0 0 0	$ \begin{array}{c} .1\\ 7.5\\ 13.4\\ 8.2\\ 3.0\\ .8\\ .4\\ .2\\ 0\\ 0\\ 0\\ 0\\ 0\\ 0\\ 0\\ 0\\ 0\\ 0\\ 0\\ 0\\ 0\\$.3 20.9 17.0 5.0 1.2 .3 .4 .1 .2 0 0	.1 7.4 10.0 2.7 .6 .1 .2 0 0 0 0	0 0 .2 .1 0 0 0 0 0 0 0		.5 35.9 40.66 16.0 4.85 1.2 1.0 .3 .2 0 0
Total % ≥ 5 feet	.21	33.6 1.4	45.4 1.0	21.1	.3 0	0	100.6 2.7
			Apri1-	Мау			
0-1 1-2 2-3 3-4 4-5 5-6 6-7 7-8 8-9 9-10 10+	0 0 0 0 0 0 0 0 0 0 0	$\begin{array}{r} .10\\ 3.31\\ 6.43\\ 4.69\\ 1.88\\ .53\\ .14\\ 0\\ 0\\ 0\\ 0\\ 0\\ 0\\ 0\\ 0\\ 0\end{array}$	$\begin{array}{r}.16\\18.57\\18.8\\5.41\\1.14\\.10\\0\\0\\0\\0\\0\\0\\0\\0\\0\\0\\0\\0\\0\\0\\0\\0\\0\\0$.04 15.69 17.74 4.96 .30 .19 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0	235 37.595 42.955 15.055 3.32 .67 .14 0 0 0

44.18

17.08 .67

0 0

Total % ≥ 5 feet 38.8 .19

0 0 0

99.34 .96

Table 9.

Table 9. (cont.)

CERC-COAST GUARD COOPERATIVE SURF OBSERVATION PROGRAM 4/54-12/65

Average Percentages for Wave Heights (rows) by Direction (columns) June-September

	North	<u>N. East</u>	East	<u>S. East</u>	South	S. West	<u>Total</u>
0-1	0	0	0	.12	0	0	.18
1-2	0	2.66	17.30	19.18	0	0	39.15
2-3	0	4.00	16.87	17.92	.03	0	38.81
3-4	.05	4.07	5.92	5.13	0	0	15.13
4-5	0	2.11	1.31	.74	0	0	4.16
5-6	0	1.13	.62	.16	.0	0	1.82
6-7	0	.89	.19	.17	0	0	,54
7-8	0	. 0	.05	.10	0	0	.12
8-9	0	0	0	.05	0	0	.06
9-10	0	0	0	0	0	0	0
10+	0	0	0	0	0	0	0
Total	.05	14.2	42.32	43,43	.03	0	100.03
≥ 5 feet	0	2.02	.86	.49	0	0	2.6

October-November

%

0-1 1-2 2-3 3-4 4-5 5-6 6-7	0 0 0 0 0 0	0 .05 .02 0 0 0 .05	.02 6.83 12.11 9.13 3.07 1.04 .81	.24 17.56 19.01 6.79 1.48 .67 .14	.11 7.19 9.53 3.05 .9 .12 0	0 0 .03 0 0 0 0	.38 31.63 40.71 18.98 5.45 1.83 .99
8-9 9-10 10+	0 0 0	0 0 0	.03 0 0	0 0 0	0 0 0	0 0 0	.02 0 0
Total % ≥ 5 feet	0	.12	33.03 1.88	45.91 .83	20.91	.03 0	100.0 2.87

Table 10.

CHESAPEAKE LIGHTSHIP 1/70-12/72

Seasonal Average Percentages for Significant Wave Heights (rows) by Direction (columns) December-March

	<u>345°-15</u> °	<u>15°-45°</u>	<u>45°-75°</u>	<u>75°-105°</u>	<u>105°-135°</u>	<u>135°-165°</u>	<u>165°-195°</u>	<u>Total</u>
<pre>< 1 1-1.5 2-2.5 3-3.5 4-5.5 6-7.5 8-9.5 > 9.5</pre>	3.1 3.7 .8 .1 .1 0 0	5.6 7.0 1.2 .2 0 0 0	3.6 6.6 .7 .2 0 0 0	2.23.9.4.20000	3.14.5.2.10000	3.6 5.4 .5 0 0 0 0	4.9 4.7 .2 .1 0 0 0	26.1 35.8 4.0 .9 .1 0 0
Tota1 % ≥ 3 meters	7.8 .2	13.9	11.0 .2	6.7	7.8 .1	9.5 0	9.9 .1	66.9 1.0
				April-May	•			
< 1 1-1.5 2-2.5 3-3.5 4-5.5 6-7.5 8-9.5 > 9.5	3.5 3.7 0 .3 0 0 0 0	$2.4 \\ 7.1 \\ .3 \\ 1.3 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ $	2.5 5.1 .5 0 0 0 0	4.2 9.6 .3 0 0 0 0 0	4.6 6.1 .7 0 0 0 0 0	7.4 11.1 .2 0 0 0 0 0	6.7 3.5 .2 0 0 0 0 0	31.3 46.2 2.2 1.6 0 0 0
Total % ≥ 3 meters	7.6	11.1 1.3	8.1	14.2 0	$11.3 \\ 0$	18.7 0	10.5 0	81.3 1.6

Table 10. (cont.)

CHESAPEAKE LIGHTSHIP 1/70-12/72

Seasonal Average Percentages for Significant Wave Heights (rows) by Direction (columns) June-September

	<u>345°-15</u> °	<u>15°-45°</u>	<u>45°-75°</u>	<u>75°-105°</u>	<u>105°-135°</u>	<u>135°-165°</u>	<u>165°-195°</u>	<u>Total</u>
< 1 1-1.5 2-2.5 3-3.5 4-5.5 6-7.5 8-9.5 > 9.5	.7 4.0 .3 0 .1 0 0 0	3.8 6.9 1.1 .1 0 0 0	4.1 4.0 1.4 .1 0 0 0	5.9 8.0 .5 .5 0 0 0	9.5 9.0 .1 0 .1 0 0	8.7 9.2 .5 .1 0 0 0	5.6 5.5 .5 .1 0 0 0	38.3 46.6 4.4 .9 .2 0 0 0
Total % ≥ 3 meters	5.1	11.8 .1	9.5	14.9 .5	18.6	18.5 .1	.1	90.4 1.1
			Oct	ober-Novembo	er			
< 1 1 -1.5	1.4 4.0	5.1 9.8	2.8 9.8	2.6 10.2	3.6 7.5	4.0 4.6	2.2	21.7 48.0

2-2.5	1.4	2.6	2.5	1.8	1.4	.3	.6	10.6
3-3.5	0	.8	.3	.6	0	.1	0	1.8
4-5.5	0	0	0	.1	0	0	0	.1
6-7.5	0	0	0	0	0	0	0	0
8-9.5	0	0	0	0	· 0	0	0	0
> 9.5	0	0	0	0	0	0	0	0
Tota1	6.8	18.4	15.4	15.4	12.4	9.0	4.8	82.2
% ≥ 3 meters	0	.8	.3	.7	0	.1	0	1.9

Table 11.

SHIP OBSERVATIONS 12/48-12/72

Seasonal Average Percentages for Significant Wave Heights (rows) by Direction (columns) December-March

	<u>345°-15°</u>	<u>15°-45°</u>	<u>45°-75°</u>	<u>75°-105°</u>	<u>105°-135°</u>	<u>135°-165°</u>	<u>165°-195°</u>	<u>Total</u>
<pre>< 1 1-1.5 2-2.5 3-3.5 4-5.5 6-7.5 8-9.5 > 9.5</pre>	3.4 6.1 1.8 .4 .05 0 0	3.4 4.8 1.2 .3 .1 .1 .05 0	2.7 4.4 1.8 .4 .2 0 .05 0	2.0 2.9. .4 .1 .05 0 0	1.6 1.7 .3 .05 0 0 0 0	2.5 2.7 .5 .2 0 0 0 0	2.6 3.5 .6 .2 .05 0 0	18.2 26.1 6.6 1.65 .45 .1 .1 0
Total % ≥ 3 meters	11.7 .45	9.8 .55	9.5 .65	5.3 .15	3.6 .05	5.8 .2	6.9 .25	53.2 2.3
				Apri1-May		• •		
<pre>< 1 1-1.5 2-2.5 3-3.5 4-5.5 6-7.5 8-9.5 > 9.5</pre>	2.4 4.0 1.0 .3 0 0 0	2.5 5.3 .9 .4 0 .05 0 0	3.4 4.6 .6 .1 0 0 0	3.4 5.2 .5 .1 .05 0 0	2.6 2.1 .3 .05 0 0 0 0	4.9 5.6 .4 .1 0 0 0	5.7 4.6 .7 .05 .1 0 0	24.9 31.4 4.49 1.1 .2 .05 0 0
Total % ≥ 3 meters	7.7 .3	9.2 .45	8.8	9.3 .15	5.1	11.0 .1	11.1 .15	62.14 1.35

Table 11. (cont.)

SHIP OBSERVATIONS 12/48-12/72

Seasonal Average Percentages for Significant Wave Heights (rows) by Direction (columns) June-September

		<u>345°-15°</u>	<u>15°-45°</u>	<u>45°-75°</u>	<u>75°-105°</u>	<u>105°-135°</u>	<u>135°-165°</u>	<u>165°-195°</u>	<u>Total</u>
	<pre>< 1 1-1.5 2-2.5 3-3.5 4-5.5 6-7.5 8-9.5 > 9.5</pre>	2.2 2.7 .4 .1 .1 0 0	2.9 3.7 1.0 .2 .1 0 0	$3.8 \\ 5.4 \\ 1.1 \\ .3 \\ .05 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\$	3.9 3.7 .4 .2 .05 0 0	3.6 3.1 .4 .05 .05 0 0 0	$ \begin{array}{c} 6.2 \\ 5.2 \\ .4 \\ .1 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \end{array} $	6.7 5.0 .4 .05 0 0 0	29.3 28.8 4.1 1.1 .35 0 0
% ≥ 3	Total meters	5.6 .2	7.9	10.6	8.3 .25	7.1 .1	11.9 .1	12.3 .05	63.65 1.45
				0cto	ober-Novembe	er			
•	< 1 1-1.5 2-2.5 3-3.5 4-5.5 6-7.5 8-9.5 > 9.5	3.1 6.0 1.7 .6 .1 0 0 0	3.15.21.7.7.2.100	3.1 5.4 1.3 .5 .1 .05 0	2.8 4.3 .7 .3 .1 0 0	2.1 3.0 .4 0 0 0 0 0 0 0 0	3.32.6.4.10000	2.9 2.2 .4 .1 .05 0 0	20.4 28.7 6.6 2.3 .55 .15 0 0
% ≥ 3	Total meters	11.4 .7	11.1 .0	10.6 .65	8.3 .4	5.5 0	6.5 .1	5.7 .15	58.7 3.0

Table 12.

SMB HINDCAST 1/48-12/50

Seasonal Average Percentages for Significant Wave Heights (rows) by Direction (columns) December-March

	North	<u>NNE</u>	NE	ENE	East	ESE	SE	SSE	South	<u>Total</u>
5-2 2-4 4-6 6-8 8-10 10-12 12-14 14-16 16-18 18-20 20-25 25-30	0 0 .04 0 0 0 0 0 0 0 0	$\begin{array}{c} 0\\.12\\.29\\0\\.53\\0\\.46\\0\\.04\\0\\.08\\.04\end{array}$	3.86 8.82 3.45 4.18 1.68 .82 .74 .61 .25 .33 .37 .08	13.8314.635.425.052.461.68.33.53.16.16.08.21	$10.48 \\ 3.08 \\ 1.35 \\ .92 \\ .49 \\ .33 \\ .08 \\ .08 \\ .04 \\ .12 \\ .04 \\ 0$	$ \begin{array}{c} 2.34\\ 1.60\\ .90\\ .27\\ .20\\ 0\\ 0\\ 0\\ 0\\ 0\\ 0\\ 0\\ 0\\ 0\\ 0\\ 0\\ 0\\ 0$	$1.02 \\ 1.02 \\ .61 \\ .25 \\ .12 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ $.41 .82 .52 .16 .08 0 0 0 0 0 0	$ \begin{array}{r} 37 \\ 20 \\ 08 \\ 12 \\ 0 \\ 29 \\ 0 \\ 0 \\ 0 \\ $	$\begin{array}{c} 32.31\\ 30.29\\ 12.62\\ 10.95\\ 5.56\\ 3.12\\ 1.61\\ 1.22\\ .49\\ .61\\ .57\\ .33\end{array}$
Total	.04	1.56	25.19	44.53	17.01	5.31	3.02	1.99	1,1	99.68
% ≥ 10 feet	0	.62	3.2	3.15	.69	0	0	0	0	7.66
					April-Mag	У				
.5-2 2-4 4-6 6-8 8-10 10-12 12-14 14-16 16-18 18-20 20-25 25-30	0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 20 0 0 0 0 0 0 0	7.07 4.61 2.15 1.13 1.02 .92 .72 .72 .10 0 0 0	$\begin{array}{c} 24.08\\ 19.26\\ 9.02\\ 3.59\\ 1.43\\ 1.22\\ .82\\ .82\\ 0\\ 0\\ 0\\ 0\\ 0\\ 0\\ 0\end{array}$	5.336.151.64.82.40.20000000	$\begin{array}{c} .61\\ 1.02\\ .20\\ 0\\ .10\\ 0\\ 0\\ 0\\ 0\\ 0\\ 0\\ 0\\ 0\\ 0\\ 0\\ 0\\ 0\\ 0$	$\begin{array}{c} & 0 \\ 1.02 \\ .20 \\ .10 \\ .20 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\$	$ \begin{array}{r} .92 \\ 1.33 \\ 0 \\ .10 \\ 0$.10 .92 .10 0 0 0 0 0 0 0 0 0 0 0 0	$\begin{array}{r} 38.11\\ 34.31\\ 13.31\\ 5.74\\ 3.35\\ 2.34\\ 1.54\\ 1.54\\ 1.54\\ .10\\ 0\\ 0\\ 0\\ 0\\ 0\end{array}$
Total	0	.20	18.44	59.42	14.54	1.93	1.52	2.35	1.12	100.21
% ≥ 10 feet	0	0	2.46	. 2.86	.20	0	0	0	0	5.52

Table 12. (cont.)

SMB HINDCAST 1/48-12/50

Seasonal Average Percentages for Significant Wave Heights (rows) by Direction (columns) June-September

	North	NNE	NE	ENE	East	ESE	SE	SSE	South	<u>Total</u>
.5-2 2-4 4-6 6-8 8-10 10-12 12-14 14-16 16-18 18-20 20-25 25-30	0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0	13.07 4.86 3.42 1.20 .84 .54 .24 .06 .30 .24 .24 .06	14.458.965.032.28.48.60.54.24.12.18.06.06	4.92 5.65 2.57 1.86 1.08 .54 .18 .06 .06 .12 .06 .06 .12	$1.62 \\ 1.74 \\ 1.44 \\ 1.08 \\ .84 \\ .72 \\ .24 \\ 0 \\ .12 \\ 0 \\ .18 \\ 0$	1.56 1.48 1.50 1.02 .84 .78 .36 .18 .06 .06 0 0	$ \begin{array}{r} 1.20 \\ 1.68 \\ .78 \\ .24 \\ .24 \\ .30 \\ 0 \\ .06 \\ 0 $	$ \begin{array}{r} .96\\ 3.37\\ .18\\ .12\\ .30\\ 0\\ .06\\ 0\\ 0\\ 0\\ 0\\ 0\\ 0\\ 0\\ 0\\ 0\\ 0\\ 0\\ 0\\ 0\\$	$\begin{array}{c} 37.78\\ 28.78\\ 14.87\\ 7.80\\ 4.62\\ 3.48\\ 1.62\\ .60\\ .66\\ .60\\ .54\\ .18\end{array}$
Total	0	.06	25.07	33.00	17.05	7.98	7.84	4.50	4.99	101.53
% ≥ 10 feet	0	.06	1.68	1.8	1.02	1.26	1.44	.36	.06	7.68
				Octo	ber-Novem	ber				
5-2 2-4 4-6 6-8 8-10 10-12 12-14 14-16 16-18 18-20 20-25 25-30	0 0 0 0 0 0 0 0 0 0 0 0 0	$\begin{array}{c} 0\\ 0\\ .20\\ 0\\ 0\\ 0\\ 0\\ 0\\ 0\\ 0\\ 0\\ 0\\ 0\\ 0\\ 0\\ 0$	7.86 5.04 2.42 1.68 .94 .20 .54 .07 .13 0 .42 .20	18.28 9.94 8.26 4.57 .67 .27 .40 .40 .07 0 0 .20	$ \begin{array}{r} 10.15 \\ 7.00 \\ 4.23 \\ 1.41 \\ .74 \\ .33 \\ .20 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \end{array} $	$\begin{array}{c} 2.42 \\ 2.28 \\ 1.21 \\ .20 \\ .02 \\ .33 \\ .20 \\ .07 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \end{array}$	$2.08 \\ .87 \\ .81 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ $.40 .20 .54 .47 .07 .07 .07 0 0 0 0	.27 .20 .07 .27 .07 .07 .07 .07 .07 .07 .07 .07 .00 .00	$\begin{array}{r} 41.46\\ 25.53\\ 17.74\\ 8.60\\ 2.51\\ 1.20\\ 1.34\\ .54\\ .20\\ 0\\ .42\\ .40\end{array}$
Total	0.	.20		43.06	24.06	6.7 3	3.76	1.75	.88	99.94
$\% \ge 10$ feet	0	0	1.56	1.14	.53	.60	0	.07	.07	3.97

Table 13.

VIRGINIA BEACH GAGE

Duration (hours) of the Highest .3% Waves

(calcul	ated)	(calculated)		(calculated)			
9.5 fe	et H _s	10.5 feet	H _s	11.5 feet	: .		
12.2′	$H_{1/10}$	13.4	^H 1/10	14.7'			
16.82 ′	H _{max}	18.6'	H _{max}	20.4′			
					Total		
December	0 hours	7.3 hours	0	hours	7.3 hours		
January	24.8	19.3	19.3		63.4		
March	6.0	6.0	0	•••	12.0		
May	12.5	0	0		12.5		
October	5.5	0	0		5.5		
Total	48.8	32.6	19.3	1	L00.7		

Total of 100.7 hours of waves between 9-12 feet H out of 32,338 hours of record, or .3%.

Table 14.

VIRGINIA BEACH GAGE

Occurence of Extratropical Storms During Period of Operation

	Date of		WI	ND	М	VAVE HEIGH	łT	Va. Beach Gage
Name	Storm	Surge	Speed (mph)	Direction	H _s	H ₁ /10	H _{max}	Operating (?)
	1/04/64	2.0'	28	W	*	*	*	\sim
	1/12/64	2.5′	42	Е	11.0	14.1	19.5	Ň
	2/12/64	2.0'	32	Е	10.0	12.8	17.7	Ĵ.
	1/16/65	4.0′	35	NE	12.1	15.5	21.5	\sim
	1/22/65	3.0′	36	E				-
	1/29/66	3.5'	37	E	11.5	14.7	20.4	\checkmark
	12/24/66	2.3	31	NE	6.7	8.6	11.9	
	2/07/67	2.7	33	NE	6.0	7.7	10,7	
	12/12/67	2.0'	30	E	1.5	2.0	2.7	
	12/29/67	2.01	31	W	6.0	7.7	10.7	.
	1/14/68	2.3	33	E	11.0	14.1	19.6	\sim
	2/08/68	2.5	30	NE	8.5	10.9	15,1	\sim
	11/10/68	4.3	34	N	8.5	10.9	15.1	\sim
	11/12/08	2.5	4 /	NE	9./	12.4	1/.1 10 E	√,
	3/02/09	0.0^{-1}	40	IN NE	10.4	13.3 15 /	10.0	√,
	11/02/09	2.5	20	NE	12.0	17.4	21.2	\sim
			Occurence	of Tropical	Storms			
			During Pe	riod of Oper	ation			
Cleo	9/01/64	1.0'	42	ESE				-
Dora	9/13/64	3.5	61	NE	12.5	16.0	22.1	~/
Gladys	9/23/64	2.2′	44	N	8.5	10.9	15,1	\sim
Isabell	10/16/64	2.5'	50	NE	9.5	12.2	16.8	, V
Alma	6/13/66	1.0'	40	N	8.0	10.2	14.2	\mathcal{A}
Doria	9/16/67	4.0′	55	N	8.0	10.2	14.2	\mathcal{I}
Gladys	10/20/68	1.3′	46	NE	8,5	10.9	15.1	\sim

*Gage was operating but record not available to author at this time

Table 15.

DECREASE OF COMPUTED WAVE HEIGHTS DUE TO REFRACTION, FRICTION AND SHOALING AT DAM NECK-VIRGINIA BEACH

(Average of 6-10 Wave Rays from Goldsmith, et al., 1974)

T = 8 seconds $H_0 = 6 \text{ feet}$ Tide = 0

	Water Depths	Northeast	East	Southeast
20	feet	1.19′	1.57'	2.18′
30	feet	1.14′	1.59'	2.33′
150	feet ("deep" water)	6.0′	6.0'	6.0′

T = 10 seconds $H_0 = 6 \text{ feet}$ Tide = 0

	Water Depths	Northeast	East	Southeast
20	feet	0.98′	1.9′	1.15′
30	feet	0.97′	2.0′	1.18′
250	feet ("deep" water)	6.0'	6.0'	6.0'

Table 16.

DAILY VOLUNTEER WAVE OBSERVATIONS AVERAGED BY SEASON

July 1974-Aug. 1976

		Wi	nter		Sp	ring		Sum	mer		Fa	.11		Total
		т	н	D°	Т	Η	D°	Т	Н	D°	т	Н	D°	# ODS.
C.	39th Street	8.09	1.97	83.44										28
eacl	73rd Street	6.54	1.68	94.54	6.66	1.72	89.06							168
nla b	Howard Johnson				7.71	1.5	100.78	÷					· ·	9
1 20 1 20	Hilton Inn							6.54	1.9	90.42	5.34	1.15	90.94	306
5	7th St.	10.84	1.93	91.08	· 9.68	2.30	91.40	10.76	2.02	98.04	10.86	2,60	91.68	341
	Dam Neck	8.66	1.52	91,33	8.6	1.32	91.4	10,50	1.97	97.52	10.32	2.13	8.55	529
	Sandbridge	9.44	1,91	93.33	8.26	2.68	87.13					1. 4. 1		39
	Beacon Rest.	7,05	1.68	38,56	8,90	1.42	36.27	8.37	2.52	93.43	9.86	1.86	94.5	268
	Back Bay	7.89	1.32	34.	7.53	1.24	48.88	7.87	3.5	84.96	4,36	1.62	27.08	120
	Currituck Beach Lt. North Carolin	na			8.11	2.25	87.78	7.72	2.22	68.05			(Total)	$\frac{74}{1882}$
					· .	T.	= Time	(seconds)		•		• •	
					·	H	= Wave	Height (feet)	(1 ft.	- 0.305	m)	•	•
						D°	= Direc	tion (de	grees:	90° =	due eas	t)	а А. Д.	





Figure 1b. Location Map

37° 00' `£J TT 1Ω (20 10 6 72 O 5) <u>36°</u> 50' BATHYMETRY OF THE VIRGINIAN SEA VIRGINIA BEACH 1973 CONTOURED IN FEET AT 3' INTERVALS √36 ୍କୁ 61 VICTOR GOLDSMITH, CAROLYN H. SUTTON, ASBURY H. SALLENGER Department of Geological Oceanography PROPOSED సి 3 18N ŕŻ 6 VIRGINIA INSTITUTE ÓF MARINE SCIENCE Gloucester Point, Virginia 23062 ζ_{s} 0 76* 00' 75° 50'

Figure 1c. Location Map





Figure 2.

DAM NECK WAVE CLIMATE SOURCES





MONTHS

COMPILED BY GUTMAN, VIMS, 10/76

H_s IN METERS



COMPILED BY GUTMAN, VIMS, 10/76



.

COMPILED BY GUTMAN, VIMS, 10/76



COMPILED BY GUTMAN



Figure 7.

COMPILED BY GUTMAN, VIMS, 10/76


WAVE HEIGHT IN METERS

Figure 8.

COMPILED BY GUTMAN, VIMS, 10/76



Figure 9.

1.)

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Figure 10.







Figure 12.



Figure 13.



Figure 14. (after Saville, 1954)

1)



Wave rays computed with following input conditions AZ = 45°; T = 8 sec; Tide = 0 Figure 15.(after Goldsmith et al., 1974)



Wave rays computed with following input conditions: AZ = 45°; T = 10 sec; Tide = 0 Figure 16. (after Goldsmith et al., 1974)







Wave rays computed with following input conditions: AZ = 90°; T = 10 sec; Tide = 0 Figure 18. (after Goldsmith et al., 1974)



Wave rays computed with following input conditions: AZ = 135°; T = 8 sec; Tide = 0 Figure 19. (after Goldsmith et al., 1974)



Wave rays computed with following input conditions: $AZ = 135^\circ$; T = 10 sec; Tide = 0 Figure 20. (after Goldsmith et al., 1974)

APPENDIX A.

COSOP Sample Wave Observer Form

•

 SURF OBSERVATION FORM (Instructions on Reverse Side)
 Cooperative Surf Observation Program
 Coastal Engineering Research Center

Sheet	Number
Statio	n

Date I	Time 2	Peri 3	od	Height 4	^D ir 5	т _{ур} е 6	Remarks 7	Observer 8
Year	0400		Τ					
	0800							
Month	1200							
	1600							
Day	2000							ه
	2400							
Month	0400							
	0800							
	1 200							
Day	1600							
	2000							
	2400							
Month	0400							
. [0800							
	1 200		Τ					
Day .	1600							
	2000							
	2400							

CERC 69 21 April 70

Signature:_

Commanding Officer

APPENDIX B.

VIMS-CERC Sample Wave Observer Form

		 In the matrix and the m				
Return to V. Goldsmith VIMS		WAVI	E OBSERVAT	ION REPORT	SITE NAM	۸ <u>۶</u>
Gloucester Pt., Va. 23062		RECO	ORD ALL DATA CAREF	ULLY AND LEGIBLY		
	YEAR MONTH DAY	TIME	WAVE PERIOD	BREAKER HEIGHT	OBSERVEI WAVE ANGLE AT BREAKER	R WAVE TYPE
		Record time Ret using the 24 hour eleve system. tiona	card the time in seconds for en (1) wave crests to pass a sta- ry point. If calm record O.	Record the best estimate of the signifi- cont wave height to the nearest half of a foot.	Record to the nearest degree the direc- tion the waves are coming from using the protractor on the reverse side.	O - Calm I - Spilling 2 - Plunging 3 - Surging 4 - Spilling / Plunging 5 - Collapsing
SITE 12345 NUMBERS		12 13 14 15			22 23 24	25
SUN						
				•		
MON						
TUE						25
WED						
ТНО			16 17 18			25
FRI						
SAT						25





APPENDIX C.

Time of Operation of Virginia Beach Gage

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•								
C' orm 174- 18 Ma COORDINATES: N	74 r 74 36 ⁰ 51' W 75	COASTAL 5°58'	ENGINEERING R .CH CEN LOCATION:1	TER WAVE 5th St.	E GAGE HISTO Fishing Pier	RΥ , Virgini	a Beach, Virgin	ia
Type of Gage	Beginning of Proper Operation	End of Proper Operation	Explanation	Gage Length (feet)	Gage Range (ft MSL)	Water Depth (ft MSL)	Distance from seaward end of pier	P Le (1
Step Resistance (SR) Staff - Parallel Type	13 Oct 62	26 Nov 62	Gage and part of pier destroyed by storm	25		18	60 (on N. side of pier)	80
SR Staff - Relay Type	2 Mar 63	17 Jan 65	Gage and part of pier destroyed by storm	25	•	18	11	80
SR Staff - Relay Type	29 Nov 65	20 Sep бб	Gage temporarily removed during pier repair	25		20	12 (on N. side of pier)	90
SR Staff - Relay Type	3 Nov 66	31 Mar 70	Recorder house vandalized	25	•	20	17	90
	22 Apr 70	26 Mar 71	Gage destroyed by storm- not replaced					
	•				•			
r 23,9,1								
		47 			·			

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APPENDIX D.

Virginia Beach Gage-Monthly Summaries

$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	#1 #100 (\$105)		HEIGHT (FT)													
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$\begin{array}{cccccccccccccccccccccccccccccccccccc$. * • 5,9 • * • • •	2 6 11	54° 54	50 37 6	22 9	11 7	2	4	2	u	,			142	654 712	2.45
1 1 1 1 2 2 2 0 157 2 50 157 2 50 157 2 50 157 2 50 157 2 50 157 2 50 157 2 50 157 2 50 157 2 50 157 2 50 157 2 50 157 2 50 157 2 3 3 2 2 3 3 2 2 3 3 2 2 3 3 2 2 3 3 3 2 2 3 3 3 2 2 3 3 3 2 2 3 3 3 2 2 3 3 3 2 2 3 3 3 2 2 3 3 3 3 3 2 2 3 3 3 2 2 3 3 3 2 2 3 3 3 3 2 2 3 3 <td>1******* 1*******</td> <td>32</td> <td>62 86 52</td> <td>. 9</td> <td>7</td> <td>222</td> <td>6</td> <td>2</td> <td>ž</td> <td>ž</td> <td>ž</td> <td>2</td> <td>2</td> <td>116</td> <td>488</td> <td>2.19</td>	1******* 1*******	32	62 86 52	. 9	7	222	6	2	ž	ž	ž	2	2	116	488	2.19
13 2,21 108 535 179 69 35 19 19 13 7 6 6 4 2,25 11 100 199 15 177 108 75 19 19 13 7 6 6 4 2,25	·* •::,9 ·* •:2,9 ·* • 1,9	4 2 2	43	1 9 7	2	2	2	4	1 2 3	z	5	2	. 5	64 97	157	2,59
		108	7 535 1892	2 179 356	69 177	35	19	19	13	7 22	8 15	6	- e 8	13	13	2,21

"AINEN FADIN FANINUTE DEN AND INK RECORDS TAKEN WITH A STEP RESISTANCE RELAY THITLD.

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·· • 1.0	9	19	15								49	983	1.64
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	9	26	40	3							91	646	1.96
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•.• 1,q	A	86	15	6	-		3	3			91	666	2.19
4	15	50	15	ğ	6	3	3				115	573	2.14
··· • • •	17		22	3	ŝ						185	458	1.50
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174 TOTAL	1000	717	26.5		3.4	22	15	- Ā	١.	ž			
- i A.,	8.808	A	7 0 1	8 4 2	8.25	10.00	7.50	7-50	- 00	6.50	8.25		
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197683 Dru			1.23	PI 50		LY-LYNAP		AVE FE					

*** CS*AINED FROM 7-HINUTE PEN AND INK RECORDS TAKEN WITH A STEP RESISTANCE RELAY **** CASE LOCATED AT 15TH STREET PIER * CALOS ARE OHITTED.

Pt P100

PERIOD (SECS)

121 OBSERVATIONS

HEIGHT (FT)

SUMMARY FOR MAR 66 MAR 68

1

12,6 = 12,9 6 21 9 2 2 2 2 44 66 1,92 13,0 = 13,9 2 11 4 9 2 20 42 2,32 14,0 = 14,9 2 9 2 14 16 2,00 1,0 = 14,9 2 9 2 14 16 2,00 1,0 = 14,9 2 9 2 14 16 2,00 1,0 = 14,9 2 9 2 14 16 2,00 2 2 5,50 - (4) 192 659 199 64 34 28 19 2 2 5,50 - (4) 192 659 199 64 20 199 64 20 199 64 199 64 199 64 199 64 199 64 199 64 199 65 199

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											1000	.00
2.9											1000	.00
	9	15								24	1000	1.10
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4.0		61	3.4	16			2			151	804	3 45
2.2 0 242										141	007	2.40
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1.5 . 7.9	6	32	51	6	11	· 6	2			91	566	2,55
6.2 . 8.9	15	43	4	2	2	5	2			77	476	\$ 77
6.0 . 9.9	17	62	24	6	4	- 2				126	199	1.85
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9	6	49	17		2		2	-		RA	172	1.62
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	š		à	2		2	•			34		111
13.0 413.4		11	-			<u> </u>				£ U	42	6136
14.0 -12.9	5	9				2				14	16	5.00
11.0 -15.9									5	2	2	8,50
1. 14L	192	659	149	64	34	28	19	2	5			1.97
	1000	808	N 1.8		n c	E .	30		5			

DAVE CLIMATOLOGY FOR VINGINIA BEACH, VINGINIA CISTRIBUTION OF SIGNIFICANT MEIGHT VS PEHIOD (IN OBSERVATIONS PER 1000 OBS) 068 DBSERVATIONS SUMMARY FUN FEB 66 FEB 67 FEU 68 048100 HEIGHT (FT)

LANE PLANEND OF FOR VIRGI	ATV HEARING ATROTAT
MAYE LLI STILL OF ATAL TI TALLT	DETCHT VS PERIDA FIN ADDEDVATIONS PER 1000 083)
DISTRIBUTTIN OF SIGNIFICAN	HEIGHT IN THIRD IT ANALYSING CONTRACTOR
AND OPELOWATIONS	SUMMARY FOR APR 64 APR 66 APR 67 APR 68
277 UPSPHERITO.0	

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(SECS)											
										CUN.	R0+
	0+1	1=2	5=3	5=4	4=5	5eb	6=7	7=8	TOT,º	101.0	AVG,#
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2.0 - 2.0	•									1000	.00
2.5 . 2.9							,			1000	.00
3.0 = 3.0	2	17	2						21	1000	1.50
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4.6 - 4.9	2	24	21	5	5				28	958	5*50
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5 A - 5 G	٦	66	37	17	2	5			132	777	5,55
7 4 - 7 9	-	63	37	10	10				121	646	2.24
	1.5	ġ.	63	9	Ż				182	525	1.08
	10	73	28	9	- 3			2	126	392	1.94
	Ľ.	5.4	\$7	2	•				98	216	1.89
1090 41094	5	28	10	10			2		56	311	2.25
11.0 011.4	5	21	12			2			39	61	2.05
16.0 416.4	£	C1	15			2			16	23	2.28
1200 01204		•	ĩ	,		ž					5.50
10.0 510.4		E 4 3	110	BA.	24	12	2	2	•	•	2.09
TUTAL		205	,55	121		16	3	ž			
CUM, TOTAL	1000			,	7.00	9.34	11.50	8.50	8.07		
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SUMMERY FOR MEY 66 MAY 67 MAY 68

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12 7 8.00 10.50

CUH. 101.8 EDE AVG.

1.50 1.50 1.50 .50 .50 1.85

7.79

0-10 10-11 11-12 TOT-F

2 9,50

.00

HEIGHT (FT)

DISTRIBUTTIN OF STGNIFICANT	SUMMARY FOR APR 64 APR 66 APR 67 APR 68	,
STA OFSEATERING	· · · · · · · · · · · · · · · · · · ·	
0.0103	HEIGHT (FT)	

AVERAGE WAVE PERIOD & 7,79 SEC VARIANCE OF WAVE PERIOD & 5,55 SEC 330 STANDARD DEVIATION OP PERICD & 2,36 SEC AVERAGE SIG, METCHT = 1,85 PT Variance of Sig, Metcht = 1,55 PT Standard Deviation of Meticht = 1,23 PT

22 5,50

36

RESULTS OBTAINED FROM 7-MINUTE PEN AND INK RECORDS TAKEN WITH A STEP RESISTANCE RELAY MAYE GAGE LOCATED AT 15TM STHEET PIER CALMS ARE DMITTED.

PERIOD (SECS)

0 =16.9 TOTAL CUM, TOTAL COL, AVG.

10.0

416 OBSERVATIONS

0=1 46

1=2

558 858 7,65

214 300 7,44

5120522

12

50 87 7:60

DISTRIBUTION OF SIGNIFICANT HELOH VIRGINIA DISTRIBUTION OF SIGNIFICANT HELOHT VS PERIOD (IN DUSERVATIONS PER 1600 085) 360 DASERVATIONS SUMMARY FOR JUN 66 JUN 67

PERIOD (SEC5)		HEIGHT (FT)										
											CUN, RC-	
	0-1	1+2	203	3=4	805	5=6	6=7	7=8	8=9	T0T.F	TOT AVOIR	
.0 . 1.9		-									1000	
2.0 - 2.4											1000	
2.5 . 2.9											1000	
3.0 . 3.4	8	6								14	1000	
1.5 . 3.9		36	5							39	986 1.52	
4.6 4.9		28			•					33	947 1.07	
5.0 . 5.9	6	28	19							53	910 1.16	
A.0 = A.9	_	64	11			3	6	6	3	56	801 5.05	
7.0 . 7.9	25	167	22	6			6	8		233	769 1,27	
8.0 o Å.9	19	183	17	-		3			3	225	536 1.62	
0 0 0 0 0	14	214	17							204	311 1.55	
A A -14.9		28	••							33	67 1.53	
1 A	ĩ	L.								11	33 1.75	
	1	ň								6	55 1.00	
		1	3							8	17 1.83	
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1480 4148*	81	778	97	6			11	14	.6		1.72	
IVIAL TOTAL	1005	0.7	. 10	n 2	86	36	τi.	19	Ā			
	1000		. 10	1 6 1	.00	7.50	7.00	7.10	7.50	7.99		
LOLS AVOS	0.014			1970								
WEBLER ETE	NETONT		2 17			VERAGE	WAVE	PESIOD	F 7.	90 550		
RECARC DID.						ADTAL!	FOFW	ANE PE	#100	1.14	5 SEC 85:	

STANDARD DEVIATION OF PERIOD # 1,92 SECH STANDARD DEVIATION UP HEIGHT & 1.14 FT

SUMMARY FOR JUL 64 JUL 65 JUL 67

PEPIDA (ELCS)				₩£ 1 G	HT (FT)				-	
							:			ÇUH,	ROM .
	0=1	1=5	5=3	3=4	805	500	6=7	7=8	T01.*	101.5	AVG
.0 - 1.5										1000	.00
2.0 - 2.4										1050	.00
2.5 . 2.9										1000	.00
3.0 - 3.4			4						4	1500	2,50
3.5 - 3.9		7	8						11	849	1,90
4.0 . 4.9		7	9	4					- 50	984	2,39
5.0 - 5.9		18	10	4	2				40	905	35,2
6.0 a 6.9	5	55	11	11	Q	11			67	925	3,03
7.0 - 7.9	16	73	42	1	2	7	4		151	858	2.13
B.0 - 8.5	40	197	39	7	9	4			295	707	1.69
9.0 . 9.9	33	182	35	4	2			5	257	412	1,51
10.0 -10.9	11	62	15	5					89	155	1.57
11.0 -11.9	ż	11	8						18	67	1.62
12.0 +12.9	4	7	5						13	49	1.35
13.0 -13.9	2	11							15	15	1.33
14.0 -14.9	2	· · · ·	9	5					20	22	2.04
15.0 +15.9	_			-						2	.00
16.0 =16.9		2							2	2	1.50
TOTAL	113	615	186	42	24	52	4	2		-	1.35
CUH. TOTAL	1000	E87	262	95	53	29	7	2			
	9.758	سلقمط	A.20	7.61	7.50	7,20	7.50	9,50	8,69		
									•		

AVERAGE WAVE PERIOD & 8,69 SEC* VARIANCE OF WAVE PERIOD = 3,61 SEC ST* STANDARD DEVIATION OF PERIOD = 1,90 SEC* AVERAGE SIG, HEIGHT # 1.85 FT VARIANCE OF SIG, HEIGHT # 1.11 FT SO STANDARD DEVIATION OF HEIGHT # 1.05 FT

RESULTS COTAINED FROM 7-RINUTE PEN AND INK RECORDS TAKEN WITH A STEP RESISTANCE RELAT WAYE GAGE LOCATED AT ISTH STREET PIER CALMS ARE OMITTED.

451 DESERVATIONS

BAVE CLIMATOLOGY FOR VIRGINIA REACH. VIRGINIA DISTRIBUTION OF SIGNIFICANT MEIGHT VS PERIOD (IN DUSERVATIONS PER 1000 ORS) BUR DISERVATIONS SUMMARY FOR AUG 60 AUG 66 AUG 67

PERIOD (SFCS)				HE I	GHT (FT)		
-							CUM.	R0=
	0=1	102	203	504	405	101.*	T01,+	AVG.+
.0 0 1.9	10						1000	.00
2.0 0 2.4							1000	.00
2.5 . 2.9							1000	.00
3.0 = 3.4		4	S			7	1000	1.63
3.5 - 3.9			4			5	953	2,50
4.0 - 4.9	5	11	9	7		29	989	2.19
5.0 = 5.9	9	22	13	9	2	57	959	2.02
6.0 = 6.9	25	58	13	7		104	902	1.52
7.0 = 7.9	50	63	11	11		161	798	1.37
8.0 . 8.9	67	129	27	0	2	234	637	1.39 .
9.0 . 9.9	18	107	35			161	404	1.60
10.0 010.9	18	42	31	11	2	107	2#3	1.90
11.0 #11.9	7	20	22	2	2	50	136	2.00
9.510 0.51	4	11	7	2	9	34	82	2.50
13.0 #13.9	43	11	Ż	ā		23	48	1.80
10.0 010.9	2	16	4	2		25	25	1.77
TOTAL	225	516	181	60	-18			1.53
CUH. TOTAL	1000	775	259	78	18			
COL. AVG.	A. 050	8.72	8,95	8.43	10,75	8,72		

LVERAGE SIG, HEIGHT = 1,63 FT VARIANCE OF SIG, HEIGHT = ,79 FT SG STANDARD DEVIATION OF HEIGHT = ,69 FT

AVERAGE WAVE PERIOD # 8,72 SEC# VARIANCE OF #AVE PERIOD # 0,89 SEC SQ# STANDARD DEVIATION OF PERIOD # 2,21 SEC#

SUMPARY FOR SEP 66 SEP 67 281 OBSERVATIONS

PERIOD (SECS)

HEIGHT (AT)

												CUH.	ROA
		0-1	1=2	2=3	3=4	4=5	500	6=7	7=8	8+9	TOT.*	TOT.4	AVG.
	.3 0 1.9	11	4		-						4	1000	1,50
	2.0 - 2.4											995	00
	2.5 . 2.9											996	.00
	3.0 . 3.4	4	11	7							22	896	1.07
	3.5 . 5.9		ij	1							14	475	2,00
	8.0 - 4.9		28	11	7	a					50	960	2.21
	5.0 . 5.9		36	14	25	11	4				90	\$10	2.74
	6.0 a 6.9	6	21	7	21	18	11	7			90	053	3.50
	7.0 - 7.9		28	15	18	14	14	14	4	4	119	730	3,83
	5.0 = 8.9	11	96	18	25	11	4			4	169	516	5.28
	9.0 . 9.9	25	125	1	1.0	4	9	4			183	442	1.79
	10.0 -10.9	18	68	11	4						101	259	1.50
	11.0 011.9	18	36	14	14	1					90	158	2.02
	12.0 012.9	đ	18	-		6		9			56	58	2.00
	13.0 013.9	11	11	11	-						32	32	1.50
20190	and the second second	-		128	135	71	36	28	4	7			2.36
	CUM, TOTAL	1000	897	904	291	146	75	39	11	7			
	COL. AYG.	10.160	8.67	7,97	7,97	7.70	7.30	A.13	7.50	8.00	84,8		
	AVERAGE STO	HETOHT :		n €T			VERAGE	h AVF	PESICO	5 A.	SI SECT		

AVERAGE SIG. HEIGHT = 2.36 FT VARIANCE OF SIG. HEIGHT = 2.42 FT 50 STANDARD DEVIATION OF MEIGHT = 1.56 FT AVENAGE HAVE PERICO = 8,51 SEC VARIANCE OF HAVE PERICO = 5,81 SEC 50% STANDARD DEVIATION OF PERICO = 2,41 SEC

RESULTS OBTAINED FPOH 7-HINUTE PEN AND INK RECORDS TAKEN WITH & STEP RESISTANCE RELAY 4AVE GAGE LOCATED AT 15TH STREET PIER • CALMS ARE OHITTED,

WAVE CLIMATOLOGY FOR VIRGINIA REACH. VIRGINIA DISTRIBUTION OF SIGNIFICANT HEIGHT VS PERIOD (IN OUSERVATIONS PER 1000 OBS) 300 ORSERVATIONS SUMMARY FOR OCT 64 OCT 67

PL9IDD (SFCS)				MEIGHT (FT)										
			77	1 - 0	0- F	6-6	4 - 7	7-8	8-0	0-10		CUH.	RO.	
	001	185	503	2.04	842	340	041	100	0	4010	10144	1000		
0 = 1,4	2											1000	.00	
2.0 . 4.4												1000	.00	
2.9 · C.											· .	1000	1.50	
3.0 4 3.4		3									2	607	- 00	
345 4 347		,	,								13	007	2.00	
			27	10	7						67	981	2.50	
5.0 - 5.0		27	\$7	10	30	10					1.10	916	3.20	
7.0 . 7.9		67	23	10	7	3		3		3	117	783	2.56	
80.89	10	87	63	i,	10	3	5				161	666	2.12	
0.0 . 9.9	50	100	20	10	. 7	-					167	505	1.05	
10.0 010.9	ÿ	63	20	7	13		3				114	338	2.24	
11.0 011.9	17	50	13	5	3				3		90	2.24	1.91	
9.51- 0.51	7	37	17	7		3					70	134	2,02	
13.0 +13.9		13	7	3							23	64	2,07	
14.0 +14.9	3	30	3								37	e ()	1,50	
15.0 015.9		3									3	- 3	1,50	
TOTAL	77	510	217	63	77	20	7	3	3	3			5.55	
CUM, TOTAL	1000	923	413	197	115	37	17	10	7	3				
COL. AVG.	10,010	0°°60	8,58	8°55	7.93	8,00	9,50	7,50	11.50	7,50	8,15			
AVERAGE SIG.	HEIGHT	s 2,2	2 11			VERAGE	WAVE	PERIOD	5 4,	15 SE	*			
VARIANCE OF	SIG, HEI	GHT 2	1.74	FT 80	V	ARIANC	E DF .	AVI. PE	P100 #	5.	77 520	50+		
STANDARD DEV	IATÍON D	F ⊨tIG	NT B	1.33 F	T 5	TANDAR	O DEVI	12110N	OF PER	ICD F	5.00	5 E C #		

SUMMARY FOR NOV 64 KUT 66 NOV 67

HEIGHT (FT)

(32(3)												ł
				- · ·			_				CUH,	₽0×
	0-1	1=2	5+3	3⇔€	4×5	500	6=7	7⇒8	6.9	TOT.*	101.4	AVG.
.0 a 1.9	17										1600	.00
5.0 = 5.6											1000	.00
2.5 + 2.9		•									\$000	.00
3.0 - 3.4	4	5								+	1000	.83
3.5 . 3.9	2	8	2							12	990	1.50
4.0 - 4.9	10	36	21	11		2				13	983	2.02
5.0 - 5.9	13	38	30	34	٥					122	961	2.31
6.0 . 6.9	11	60	23	11	11	10	2			112	770	2.60
7.0 . 7.9	Å	12	32	10	Ĩ.	•	-		2		61.9	2.50
5.0 p 8.9	17	A.7	27	••	Ň		•		•		573	1 71
0.0 . 0.0		00	30		Š						513	1 63
10 0 -10 0	17		30	2	E				• •	100	100	1 72
11 0 -11 0	.,	25	10	-						100	200	1 1 1 3
		22								60	101	1.4
12.5 412.44	6	· · · ·	15	5						44		1.80
1260 41284				2	9					14	33	2.74
10.0 -10.4	<u> </u>	13	£	2						19	19	1.70
TOTAL	137	497	535	78	65	11	6		5	•		1,96
CUN, TOTAL	1000	863	371	139	61	19	8	5	5			
COL, AVG,	8,13*	8.90	8,33	6.74	8,41	6.17	7.17	.00	7,50	6,44		

AVERAGE SIG. HEIGHT > 1.96 FT VARIANCE OF SIG: HEIGHT = 1.26 FT SO SIANDARD DEVIATION OF HEIGHT = 1.12 FT AVERAGE WAVE PERIOD B 8,44 SEC+ VARIANCE OF WAVE PERIOD E 6,53 SEC 80B STANDARD DEVIATION OF PERIOD E 2,55 SEC+

RESULTS OBTAINED FROM 70MINUTE PEN AND INK RECORDS TAKEN WITH A STEP RESISTANCE PELAY Have gage located at 15th street pier 8 Calms are chitted.

526 OBSERVATIONS

PERIOD

WAVE CLIMATCLOGY FOR Y	INGINIA BEACH, VINGINIA	
DISTRIBUTION OF SIGNIFI	CANT HEIGHT VS PEHICO EIN	DUSERVATIONS PER 1000 DB3)
606 OBSEMVATIONS	SUMMARY FOR DEC 6	W DEC 65 DEC 60 DEC 67

PERIOD (SECS)		HEIGHT (#Y)												
	01		7-1	t-0	0-5		A-7	7~A	8-0	6-14	10-11		CUH.	80=
	ړ- ۷ د	1.05	2.13		,	3-0	007		0	4.10	10011	101**	10140	
.0 . 1	E.			¢.								c	1000	3,30
2.0 . 2.4													448	.00
2.5 0 2.0														.00
3.0 0 3.0	<u>د</u>	13	7									15	VVB	3.34
3.5 . 3.4	3											31	463	1.01
a.o • • • •		10	23			E.						68	952	2.33
5.0 9 7.4	-		20	50	12							117	958	2.74
0,0 - 0,V		35	20	17	15		,		-			116	767	2,73
7.0 - 7.0	12		23	с -			-		c			16	673	5.21
6.0 . 8.9	10	. 30	23	6	2				-		٤	100	555	5 11
9,0 × 9,9	20	101	40	10		2	e		2			165	480	1.13
10.0 =10.9	14	0 A	26	7	3							t5 u	300	1.75
11.0 #11.9	13	46	20	3								P. S	160	1.16
15.0 015.6	2	28	15	3								51	53	1,95
13.0 013.9		13	10		5							35	66	5.56
14.0 014.9	5	2	13									17	18	5,20
15.0 015.9													2	.00
10.0 =16.7					2							5	Ż	4,50
TOTAL	109	465	251	94	50	20	7		3	÷	5	-		2.13
EUF. TOTAL	1000	891	- 426	175	61	31	12 -	5	5	Ś	5			
CUL. AVG.	8.75*	8,77	8,92	7,51	6.83	7.00	7.75	.00	8,50	.00	8,50	8,55		

AVERAGE SIG, HEIGHT # 2,13 FT AVERAGE WAVE PERIOD # 8,56 SEC VARIANCE OF SIG, HEIGHT # 1,56 FT SG VARIANCE OF HAVE PERIOD # 2,67 SEC STANDARD DEVIATION OF HEIGHT # 1,25 FT STANDARD DEVIATION OF PERIOD # 2,67 SEC#